

FINAL REPORT

LOW-DENSITY PHENOLIC NYLON NOSECAP
SCOUT REENTRY HEATING PROGRAM
REENTRY E

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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
LANGLEY RESEARCH CENTER • HAMPTON, VIRGINIA

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This report describes the development, fabrication and assembly of two charing ablator nose caps for the Scount Re-entry E Project. Also, included is the detailed design and fabrication of the nose cap instrumentation.

The material which was chosen for the experiment is a low-density phenolic nylon charring ablator. The ablator composition is a mixture of phenolic resin, phenolic microballoons, and powdered nylon. In an effect to establish a predictable material behavior, various compositions of this material were subjected to ground tests. As a result of the ground tests, the exact material composition used for this experiment has demonstrated the capability of providing an ablator with char integrity, and a predictable surface recession rate. The characteristics of this ablator resin system, when correlated with reentry data, will provide a sound basis for predicting materials behavior during reentry environments.

author

ABSTRACT FOR NASI-4141-16

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FINAL REPORT

LOW-DENSITY PHENOLIC NYLON NOSECAP SCOUT REENTRY HEATING PROGRAM

REENTRY Æ

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(PHILCO)

Contract NAS1-4141-16

Prepared for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

Langley Research Center Langley Station Hampton, Virginia

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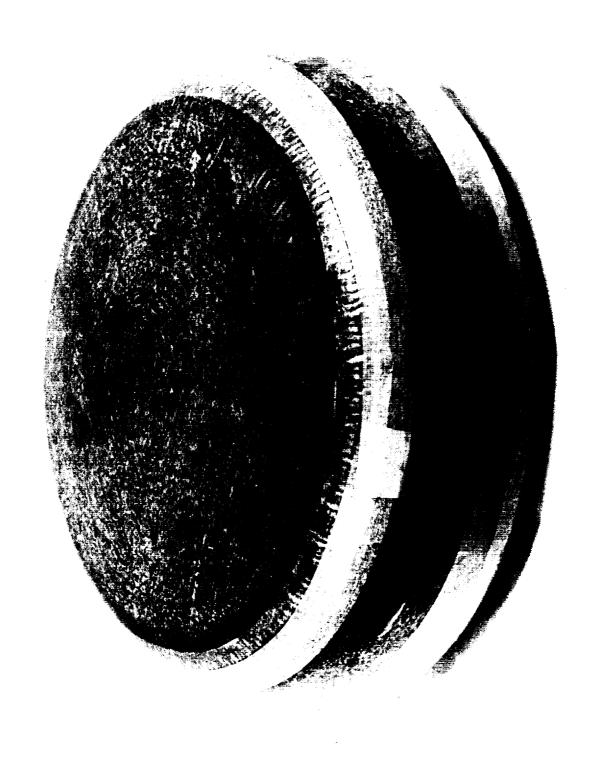


Figure 1. Reentry E Phenolic Nylon Ablative Nosecap with Moisture Barrier.

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INTRODUCTION

The Scout Reentry Heating Program consists of five models. Four models have been flown; the current model is an ablative materials experiment and is designated Reentry E. This report describes the development, fabrication, and assembly of two nosecaps for the Reentry E materials experiment. Nosecap No. 2 is the flight ready model and No. 1 is the backup.

A prerequisite for the Reentry E experiment was to select an ablative material for the nosecap which had been extensively tested in ground facilities and whose properties were sufficiently understood to make reasonable an extrapolation to the severe conditions of flight reentry.

The material which was chosen for the experiment is a low-density phenolic nylon charring ablator. The ablator composition is a mixture of phenolic resin, phenolic microballoons, and powdered nylon. In an effort to establish a predictable material behavior, various compositions of this material were subjected to ground tests. As a result of the ground tests, the exact material composition used for this experiment has demonstrated the capability of providing an ablator with char integrity, and a predictable surface recession rate. The characteristics of this ablator resin system, when correlated with reentry data, will provide a sound basis for predicting materials behavior during reentry environments.

Transducers, precisely located in the nosecap experiment, are used to provide a means of measuring the temperature and surface-recession rate of the ablator during reentry. Figure 1 illustrates the phenolic nylon nosecap with moisture protection.

DESIGN

The spacecraft systems, figure 2, used in the Scout Reentry Heating Program, while similar in design, have variations in the nosecap depending on the particular experiment. In general, the spacecraft consists of a 9° blunt-cone configuration approximately 3-feet long, with a nose diameter of about 11 inches, and a base diameter of 20 inches. The ablator for this experiment, supported by a tungsten substructure which is used to secure the nosecap to the payload, has a spherically shaped surface with a 17.4-in. radius of curvature which is blended to the 9° cone.

Reliability and Quality Assurance

The reliability and quality assurance plan for the Reentry E experiment, consisted of adherence to detailed fabrication procedures. These procedures were specifically generated for this ablative nosecap experiment and are included in the fabrication section of this report. Implementation of these procedures provided control in the areas of raw materials, fabrication, inspection, tests, and records.

A material review board consisting of project personnel was in force throughout the nosecap fabrication. The responsibilities of the review board included the control of nonconforming material and preliminary review action. In addition, the material review board controlled all drawing and procedural changes.

All material, parts, and components were procured in accordance with specifications established by the cognizant design engineer. The material specifications were recorded on the procurement documents.

A design review board consisting of nonproject personnel conducted reviews, as required, to evaluate the reliability criteria and to ensure prompt implementation of any changes that might be necessary.

Final verification of the reliability and quality assurance plan shall be ascertained when the nosecap-payload assembly and backup nosecap are subjected to the flight environmental test plan. This test plan requires the nosecap-payload assembly and the backup nosecap prototype assembly to be subjected to the expected flight environment, which includes shock, vibration, altitude, spin, and steady-state simulation. The nosecap payload and backup nosecap, upon successful completion of the flight test plan, will have satisfied all the requirements of the reliability and quality assurance plan.

Ablator Material

To obtain a phenolic nylon ablative material with char integrity and a predictable surface-recession rate, a composition of 40-percent powdered nylon, 25-percent phenolic resin, and 35-percent phenolic microballoons was formulated. This composition, when molded in accordance with Molding Procedure 104, provided an ablator material with a density of 35 ± 1 lb per cubic foot. When subjected to arc-jet tests, specimens of the ablator material satisfied the material requirements of this experiment based on analytical procedures.

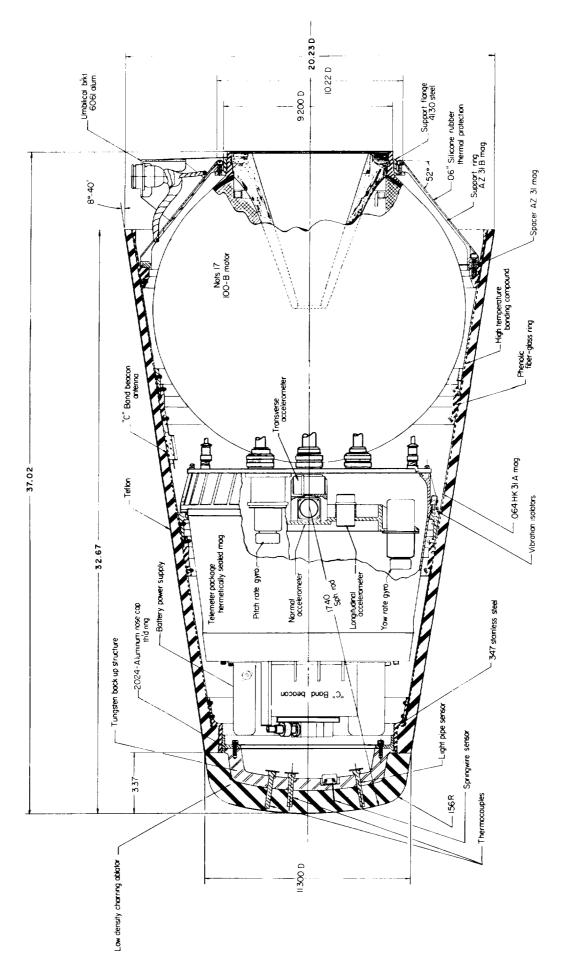


Figure 2. Reentry E Spacecraft.

The ablator material was then molded, in accordance with Procedure 104, into a 12-in. diameter billet 4-1/2-in. thick. After molding, the billet was subjected to radiographic inspection to determine whether any voids, porosity, or foreign material were present within the billet. The billet was then contoured on one side, to fit the substructure, in preparation for the bonding operation. The contouring of the ablator interface is shown in figure 3.

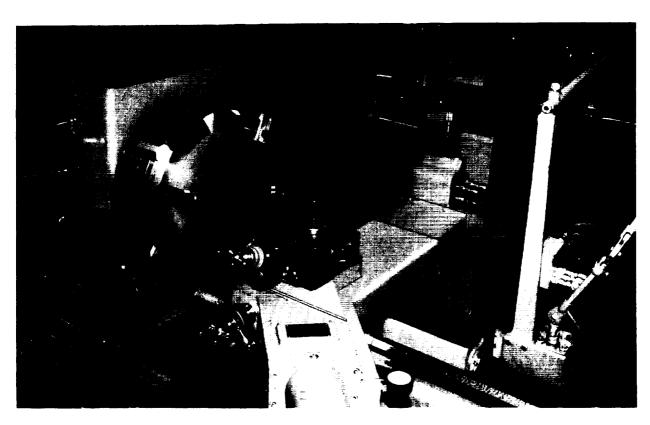


Figure 3. Ablator Interface Contour.

A 3.30-in. diameter disc (dwg No. LC-410120) was removed from the excess material contained in the billet prior to the contouring operation. This disc was then machined to provide three 1-1/2-in. diameter arc-jet specimens (dwg No. LB-410317). These specimens were then subjected to the arc-jet tests to verify that the material would perform in a manner comparable to material selected from previous arc-jet tests. After contouring of the interface area (dwg No. LC-410120), the billet was placed in a controlled environment of 70-percent +10 percent relative humidity and a temperature of 75° to $\pm 25^{\circ}$ F to stabilize the ablator material. All subsequent fabrication processes utilizing the ablator material

were performed under controlled conditions to maintain material stabilization.

Bonding of the ablator material to the substructure was accomplished in accordance with Procedure 105 using a tape-supported adhesive, HT424. This adhesive is made by the Bloomingdale Rubber Company.

After the ablator had been bonded to the substructure, the outer spherical surface of the nosecap was contoured (dwg No. LC-410120). The conical sides and the blend radius were machined to conform to the experiment requirements. After this contouring operation, a moisture barrier was applied to the nosecap in accordance with Procedure 105. This moisture barrier is a covering of 0.003-in. teflon. The teflon, manufactured by Dow-Corning, is bonded to the nosecap with DC-274 adhesive, which cures at room temperature.

Substructure

A tungsten alloy, Kennertium W-2, was chosen for the nosecap substructure to provide the spacecraft assembly with the required center of gravity. The substructure was contoured in accordance with dwg No. LC-410116, the axes were defined and inscribed on the nosecap mounting surface. As a reference indicator, thermocouple hole No. 19, contained in the vertical axis, was located nearest, and directly below, the inscribed legend "TOP". All holes required for installation of the sensors and mounting of the substructure were drilled prior to bonding of the ablator. This was done to allow a lubricant to be used during the substructure machining operation, in order to prevent the embedment of metal particles in the ablator material. All sensor installation holes were drilled with the hole axis normal to the outside contour of the substructure's spherical surface. The drilled substructure is shown in figure 4.

Helicoil inserts were placed in the sensor mounting holes to provide a positive method of securing the sensor mounting brackets to the substructure. The mounting washers for the thermocouples and light-pipe sensors (dwg No. LB-410124) were precision-ground at the time of sensor installation to ensure proper bottoming of the sensors in the ablator material. Shims (dwg No. LB-410123) were provided as required for installation of the spring-wire sensors. Bottoming of the sensors was accomplished with the use of the sensor mounting screws to apply a slight pressure on the sensor.

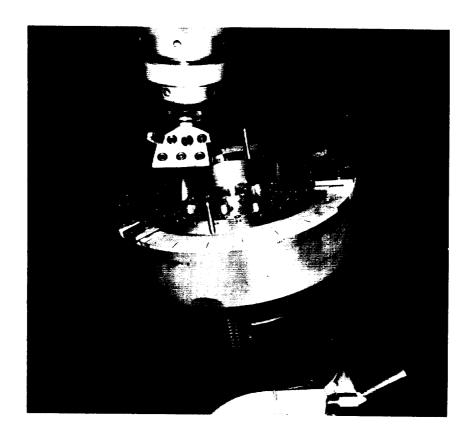


Figure 4. Drilled Tungsten Substructure.

INSTRUMENTATION

There are four types of sensors installed in the ablative nosecap. These sensors are used to measure the substructure temperature, the temperature of the ablator material, and the ablator surface-recession rate. These measurements are recorded during reentry of the experiment payload.

Substructure Temperature Sensors

Two thermistors were mounted directly on the rear surface of the tungsten substructure with RTV-102 sealant. One thermistor is mounted at the center of the substructure, and the other is mounted on an approximate 3-in. radius to provide temperature-monitoring of the rear surface area of the substructure (see dwg No. LX-410115).

Thermocouple Sensors

To determine the temperature of the ablating material, 27 thermocoupler sensors (figure 5) were installed at various depths within the ablator. The thermocouples were mounted on three concentric circles, as shown on dwg. No. LX-410115. After installation of the 27 original thermocouple sensors was completed, it was decided to install two additional thermocouples to monitor the temperature of the ablating material in the area where the blend radius connects the spherical radius to the sides of the nosecap. The two new thermocouple sensors (T/C 46 and 47) were located as shown on dwg No. LX-410115. This increased the number of thermocouple sensors to a total of 29.



Figure 5. Thermocouple Sensor.

The thermocouple assembly (dwg No. LD-410117) consists of a 36-gage resistance lap-weld chromel-alumel hot junction which provides accurate temperature indications in the ablative material. The lap weld is centered on a 1/4-in. diameter plug of ablative material. The 36-gage wires run across the end of the plug, which is an isothermal plane, in order to minimize error in the thermocouple indication due to conduction down the leads. The 36-gage wires are inserted in quartz tubing that is bonded with Shell Epon 931 in grooves placed on each side of the thermocouple plug. The quartz tubing insulates the thermocouple wires in the radial direction. To provide flexural strength for the lead wires during handling, 30-gage chromel-alumel lead wires are resistance-welded to the 36-gage wires directly behind the quartz tubing. These

wires are bonded with Shell Epon 931 in the plug grooves. A cap of ablation material is also bonded to the rear-end of the plug to secure the sensor leads. The thermocouple sensors were fabricated and tested in accordance with Procedure 103.

Light Pipe Ablation Sensors

The light pipe ablation sensor (figure 6) is designed to measure ablator surface position and, when correlated with time, to provide the surface recession rate. Four light pipe sensors are embedded at various depths within the ablative material. The light pipe sensor utilizes a high melting-point sapphire optical fiber to channel the light present at the surface of the ablating material through an infrared filter to a photosensitive diode. A predetermined diode resistance level, selected experimentally, is used to correlate surface position with time.

The light pipe sensor assembly (dwg No. LD-410118) consists of a 0.016-in. diameter sapphire rod inserted into a thru—hole in a 1/4-in. diameter plug composed of ablative material. An infrared filter, 0.082-in. diameter, is inserted into the hole from the rear of the plug and positioned flush with the sapphire rod. The photosensitive diode, with shielded leads, is bottomed against the filter. The rear of the sensor plug is filled with an epoxy resin consisting of 60-percent CIBA 6005 and 40-percent Versamid 140, which encapsulates the diode and lead wires within the plug. The light pipe sensors were fabricated and tested in accordance with Procedure 102.

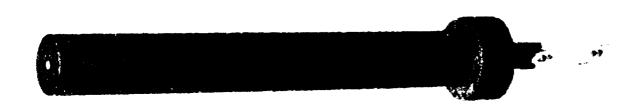


Figure 6. Light Pipe Ablation Sensor.

Spring Wire Ablation Sensors

The spring wire sensors (figure 7) were designed to obtain a measurement of the ablating material surface position which is correlated with time to yield surface recession rates. Twelve spring wire sensors are embedded at various depths within the ablator. The sensors are located on two concentric circles, as shown in dwg No. LX-410115.

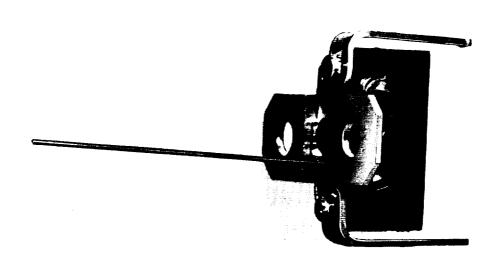


Figure 7. Spring Wire Ablation Sensor.

The spring wire sensor consists of a 0.020-in. outside-dia-meter metal tube attached to a snap-action microswitch. A 0.003-in. diameter tungsten wire, knotted at one end. is secured to the end of the tubing. which has been spun closed and drilled to a 0.004-in. diameter hole. The wire is threaded through the tubing and attached to the leaf spring of the switch so as to hold the spring under tension. The tubing is then embedded in the ablation material to the desired depth. As the nosecap material ablates to the location of the sensor, the very steep temperature gradient at and just below the surface softens the tubing and releases the wire, allowing the microswitch to close.

The choice of material for the support tube is dictated by the expected surface temperature of the ablator. For the Reentry E experiment, molybdenum (melting temperature approximately 4700° F) was selected for the support tube, and 0.003-in. diameter tungsten wire for the spring wire. The spring wire sensor assembly is shown on dwg No. LD 410119. The sensors were assembled according to Procedure 101.

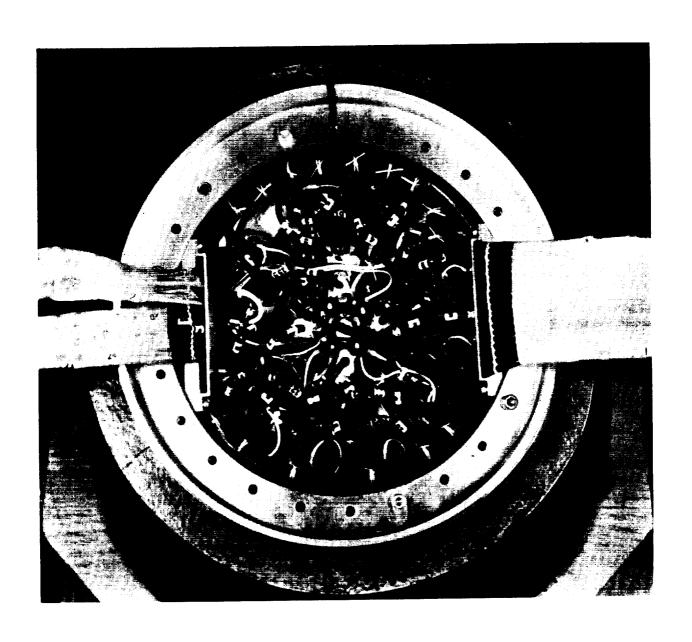


Figure 8. Nosecap Assembly with Sensing Devices.

INSTRUMENTATION INSTALLATION

The low-density phenolic nylon nosecap subassembly was supported during installation of the sensing devices to prevent damage to the ablator surface. A number of transducers are located within 0.200 in. of the forward face of the ablator; therefore, to prevent shearing of the ablator material upon insertion of the sensing devices a backup support surface was required. This support was fabricated by the use of quick-setting plaster molded to the nosecap spherical surface. The ablator material was protected from the plaster by a 0.003-in. layer of teflon. All sensors were installed in the nosecap assembly in accordance with Procedure 106. Thermocouple location hole No. 19 is adjacent to the reference point "TOP", which is inscribed on the substructure as previously described.

The spring wire ablation sensors were installed in the nose-cap assembly first, to avoid interference with other instrumentation lead wires. Nonmetallic shims are used to position the spring wire sensors within the ablator at precise depths and to prevent the sensor terminals from making electrical contact with the substructure. A shim was selected for a sensor by first measuring the depth of the hole in the ablator as well as the length of the sensor probe. Then the thickness required was computed, and the shim was machined to this dimension. The shim was placed under the mounting bracket, and the tube assembly inserted into the ablator. The mounting bracket of the sensor was secured to the substructure with mounting screws.

The thermocouple sensor assembly utilizes precision-ground washers, individually machined for each thermocouple assembly by measuring hole depth and sensor length, to assure proper bottoming of the sensor with the ablator at a specific location. Prior to insertion of the thermocouple assembly in the ablator, a thin coating of epoxy bonding agent (60-percent CIBA 6005, 40-percent Versamid 140) was applied to the sides of the thermocouple assembly plug, from the shoulder to the face end. No adhesive was applied to the face area of the thermocouple assembly. Then the sensor was inserted into the ablator and the precision retaining washer was properly positioned and secured to the substructure with mounting screws. A small amount of RTV-60 was applied to the back of the washer to support the wiring as it passes through the washer er.

The light pipe sensors were installed using precision-ground washers to assure proper bottoming of the sensor within the ablator at a specific location. A thin coating of epoxy bonding agent (60-percent CIBA 6005, 40-percent Versamid 140) was applied to the sides of the sensor from the shoulder to the sensor face end prior to insertion of the sensor into the ablator. No adhesive was

applied to the face area of the light pipe sensors. The sensor was then inserted into the ablator. The precision-ground washer was properly positioned and secured to the substructure with mounting screws. A small amount of RTV-60 was applied to the back of the washer to support the wiring as it passes through the washer. Any void between the structure and the shoulder of the light pipe sensor was filled with Epon 931. Figure 8 shows the nosecap assembly with all sensing devices installed.

Two thermistors to monitor the tungsten alloy substructure temperature were bonded to the surface of the substructure with RTV-102 sealant, as described in Procedure 106.

The common lead-wire connections were completed, the lead-wires were color-coded, and the leads were dressed and secured with cable clamps. The nosecap was then X-rayed and inspected for voids. Next, the sensor leads were wired to the connectors as indicated in table 1.

Figure 9 shows the location of thermocouple mounting holes No. 46 and No. 47. These two thermocouples were added after the nosecaps were instrumented and are used to monitor the temperature at the 9° blend radius of the nosecap. Figure 9 (sheet 2) shows the thermocouple installed in location hole No. 46.

Table 1. Connector and Sensor Lead Connections

Connector	Sensor	Pin No.	Connector	Sensor	Pin No.
P610	SW 30 31 32 33 34 35 36 37 38 39 40 41 SW Common LP 42 43 44 45 LP Common	14 15 16 17	P611	TC 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 26 Thermistor	1-2 3-4 5-6 7-8 9-10 11-12 13-14 15-16 Spare 19-20 17-18 21-22 23-24 25-26 27-28 29-30 31-32 33-34 35-37 36 (Spare)
P612	TC 46 20 21 22 23 24 25 27 28 29 47 Thermistor	1-2 Spare 3-4 5-6 7-8 9-10 11-12 13-14 15-16 Spare 19-16 17-18	pi	Thermistor- disconnect Thermistor 1 Thermistor 2 or TC pins, even negative, er pins position	odd num-

After the sensor leads were wired to the connectors (dwg No. LL-604108 and LC-603899), a resistance measurement was made of each sensor to assure satisfactory operation. These measurements were recorded on the sensor log, forms RE1, RE2-1, RE3, and RE4.

A polystyrene compound, Isofoam PE-2, was then applied to the instrumentation area of the nosecap assembly to completely encapsulate the sensors. When the encapsulant had completely cured, a resistance check of all the sensors was again performed to make sure that all sensors were functioning properly.



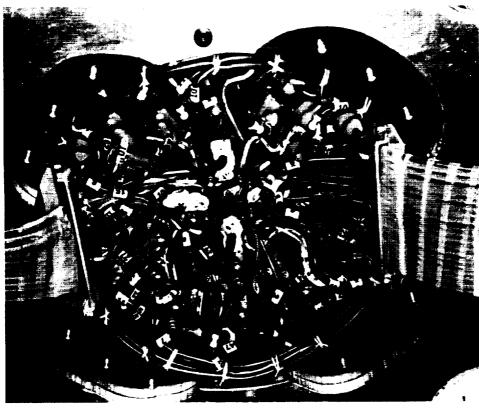


Figure 9. Location of Thermocouples No. 46 and No. 47 (Sheet 1 of 2)

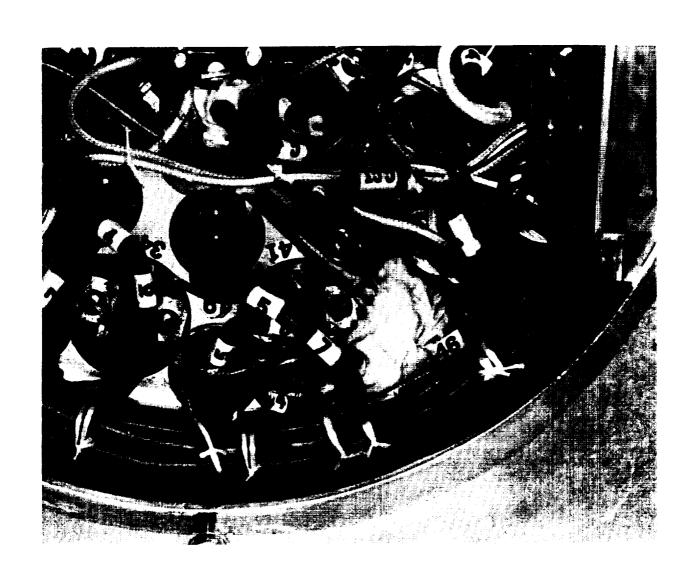


Figure 9. Location of Thermocouple No. 46 (Sheet 2 of 2)

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FABRICATION AND TEST PROCEDURES

FABRICATION AND TEST PROCEDURES

The following procedures have been developed for the Scout Reentry Heating Project Reentry E materials experiment. These procedures provide detailed guidance in component fabrication, testing, and assembly of the low-density phenolic nylon ablative nosecap.

Procedures or, Procedure 101

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SPRING WIRE ABLATION SENSOR

PROCEDURE 101

Spring Wire Ablation Sensor Assembly

The procedural steps required to fabricate the spring wire ablation sensor are given below.

- 1. Reference Drawings:
 - (a) Detailed assembly (dwg No. LD-410119) figure 12
 - (b) Locating jig (dwg No. LA-410333)
- 2. Material Required:
 - (a) Microswitch 1SM1
 - (b) Molybdenum tube, assembly drawing, detail b
 - (c) Stainless steel tubing, 0.015 in. OD X 0.011 in. ID
 - (d) Wire, 99.7 percent tungsten, hard drawn, fine grained; 0.003 in. diam., minimum tensile strength 400,000 psi, cleaned
 - (e) Switch cap, assembly drawing, detail d
 - (f) Mounting bracket, assembly drawing, detail a
 - (g) Wiring lug, assembly drawing, detail c
 - (h) RTV 102 sealant
 - (i) Duco cement
 - (j) 100K, 1/10 W, 5 percent carbon resistor
- 3. Fabrication and Test Equipment Required:
 - (a) Eye loupe, approximately 3X
 - (b) Simpson VOM, Model 262
 - (c) Spring tension gage, graduated from 50-250 grams
 - (d) 0.025-in. feeler gage
 - (e) 0.060-in. feeler gage
 - (f) Die plate, 1/16-in. thick
 - (g) Resistance welder, Unitek Weldmatic, Model 1016
 - (h) Shop microscope with eyepiece calibrated in thousandths
 - (i) Location jig

Assembly and Inspection Procedure

- 1. Remove original cover from microswitch at glue line by cracking and chipping cover. Next, remove a sufficient amount of the switch shoulder opposite the brass support plate to provide an optical sighting port for the contact leaf spring.
- 2. Clean retaining shoulder of microswitch until free of cement, residue and remaining pieces of cover.

- 3. Visually inspect microswitch to ensure that contact leaf spring of switch is free of damage and centrally aligned.
- 4. Remove the raised letters from the base of the microswitch to provide a flat measuring reference point.
- 5. On the solder lug side of the microswitch base, using the location jig shown on dwg No. LA-410333, drill a 0.020-in. diameter (No. 76 drill) hole to a depth of 0.150-in. Measure actual depth of hole and record on fabrication log, form RE2-1, figure 10.

CAUTION

Provide backup support for the contact leaf spring while drilling to prevent damage.

- 6. Drill a 0.0135-in. diameter (No. 80 drill) hole, centered in the 0.020-in. diameter hole previously drilled, through the switch base, the brass support plate, and the contact leaf spring.
- 7. Remove all burrs from the brass support plate and contact leaf spring after drilling.
- 8. Thread a knotted wire through the contact leaf spring and switch so that the tension in the spring can be measured at the location of the 0.0135-in. hole. Pulling on wire will depress switch; releasing wire will return switch to its normal position. The releasing tension is critical and must be at least 100 grams. Measure this tension with a tension gage, and record the result on the log, form RE2-1. If below 100 grams, the tension may be increased by depressing the brass support plate.
- 9. Travel is the distance which the wire will move from the fully depressed position of the spring to the point where the switch snaps back to its normal position. This travel shall be a minimum of 0.013 in. Measure and record the travel on form RE2-1.
- 10. Using a 0.060-in. feeler gage, adjust the outer contact so that the gap between contacts is 0.060 in.
- 11. Assign a serial number to the switch, and record the number on the fabrication log, form RE2-1.
- 12. Visually inspect the microswitch after drilling and make the following observations:
 - (a) Microswitch shall be free of dust and filings.
 - (b) Hole in brass support plate and contact leaf spring shall be free of burrs.

- 13. Select finished molybdenum tubing as shown on assembly dwg No. LD-410119, detail b. Measure and record the actual tubing length.
- 14. Press the tubing into the 0.020-in. diameter hole in the switch base until it is bottomed in the hole. Measure the remaining length of the tubing from the solder lug side of the switch base to ensure that the tube is bottomed; then record this length on the log.
- 15. Cut the 0.003-in. diameter tungsten wire to a length of 4 inches. Tie a simple knot in one end of the wire, and draw the wire through a 0.004-in.hole in a tempered steel die plate to set knot firmly. Use a tension of 600 grams to avoid stressing wire.
- 16. Visually inspect the wire and knot for damage using the eye loupe.
- 17. Thread the free end of the wire through the molybdenum tube, switch base, support plate, and leaf spring.
- 18. Slide a piece of stainless steel tubing onto the free end of the wire. Position the tubing close to the leaf spring. Crimp tubing to the wire.
- 19. Depress the contact leaf spring to the brass support plate, taking care to permit 0.002 to 0.005-in. clearance between spring and plate. Pull the wire taut, so that the knotted end is against the molybdenum tube. Holding the wire taut with a force of 200 grams, slide the crimped tube against the depressed leaf spring.
- 20. Adjust the dial setting of the resistance welder to 1.5-2.0 watt-seconds. Using copper electrodes, prepare a weld schedule for the tungsten wire and stainless steel tubing before making the actual weld.
- 21. With the wire held taut with 200 grams tension as in step 19, weld the crimped tubing to the wire. Trim excessive wire and tubing close to the weld junction to eliminate the possibility of interference with the action of the switch. Make a second weld to ensure that the tubing is securely fastened to the wire.
- 22. Visually inspect the assembly and make the following observations:
 - (a) Using an eye loupe, check the knot in the tungsten wire for damage.
 - (b) Using an eye loupe, inspect the weld for excessive burning.

- (c) Using a nonabrasive probe, apply just enough pressure on the leaf spring to open the contacts. Repeat this operation several times to assure that the crimped tubing is securely fastened to the wire.
- (d) Measure the clearance between the contact leaf spring and brass support plate with a shop microscope having an eyepiece calibrated in thousandths of an inch. This clearance shall be 0.002 to 0.005 in. Record the actual clearance on the fabrication log, form RE2-1.
- (e) Record the results of these inspections on the log.
- 23. Cement a bakelite switch cap onto the microswitch, using a minimum of Duco cement and taking care to avoid having cement run into the microswitch.
- 24. Attach two mounting brackets to the assembly with appropriate hardware, as shown on the assembly drawing.
- 25. Bend wiring lugs to the profile shown in the assembly drawing, and fit the lugs to the switch solder terminals.
- 26. Attach a 100K, 1/10-watt resistor between the solder terminals. Soft-solder the lug and resistor lead to the terminal. Inspect the solder connections and record the results on the log, form RE2-1.
- 27. Using red paint, mark a dot on the top of the switch cover to indicate the common terminal or side of the switch. Refer to the assembly drawing.
- 28. Using a Simpson Model 262 VOM, perform a continuity check between the wiring lugs. The sensor resistance shall be 100K +10K. Record the actual resistance on the log.
- 29. Inspect the switch cover. The seam shall be free of excess cement.
- 30. At the time of installation of the spring wire ablation sensor in the nosecap, record all pertinent data on installation log, form RE2-2, figure 11.

RETARKS INSTALLED IN POST-INSTALL CHECK PRE-INSTALL CHECK ASSEMBLY DRAWING NO LD410119 PERTODIC CHECKS RESTS FOR AND LUG SOLDER INSPECTION FABRICATION LOG SENSOR SPRING WIRE ABLATION SENSOR SENSOR LENGTH AFTER ASSY SPRING - UPPORT PLATE (LEAR INCE WELD AND KNOT INSPECTION O TUBE LENGTH INSTALLED ASSEVBLY DATE TUNGSTEN WIRE PR NUMBER PR LENGTH MOLYBDENUM TUBE FREE TRAVEL BEFORE HELLASE VICROSMITCH ISSI ACTUAL HOLE DEPTH RELEASING SPRING TENSION (GRAVE) PROCEDURE NO 101 SERIAL NUMBER

SHEET - OF _

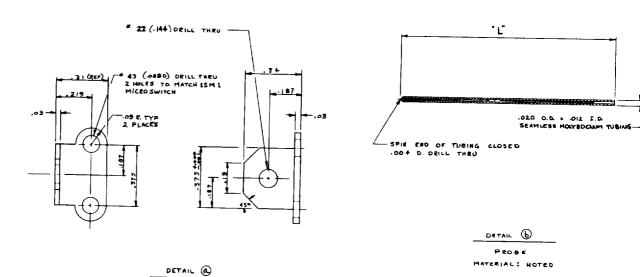
e 10. Spring-Wire Ablation Sensor Fabrication Log Figure 10.

FORW RE 2-

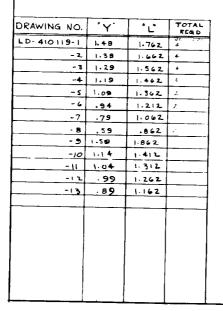
	;	Hole number	
Installed		Distance from surface to end of tube	
LOG	Date:	Shim thickness	
WIRE ABLATION SENSOR INSTALLATION LOG		Remaining thickness	
ENSOR IN	· o	Hole depth	
ABLATION S	NOSECAP NO.	Total thickness of nosecap	
		Hole	
SPRING		Length To end of knot	
		Sensor To end of tube	
		Sensor	

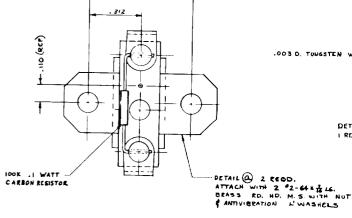
Spring Wire Ablation Sensor Installation Log. Figure 11.

Form RE2-2



MOUNTING BRKT.
MATERIAL: 2024 -T4 ALOM ALLOY





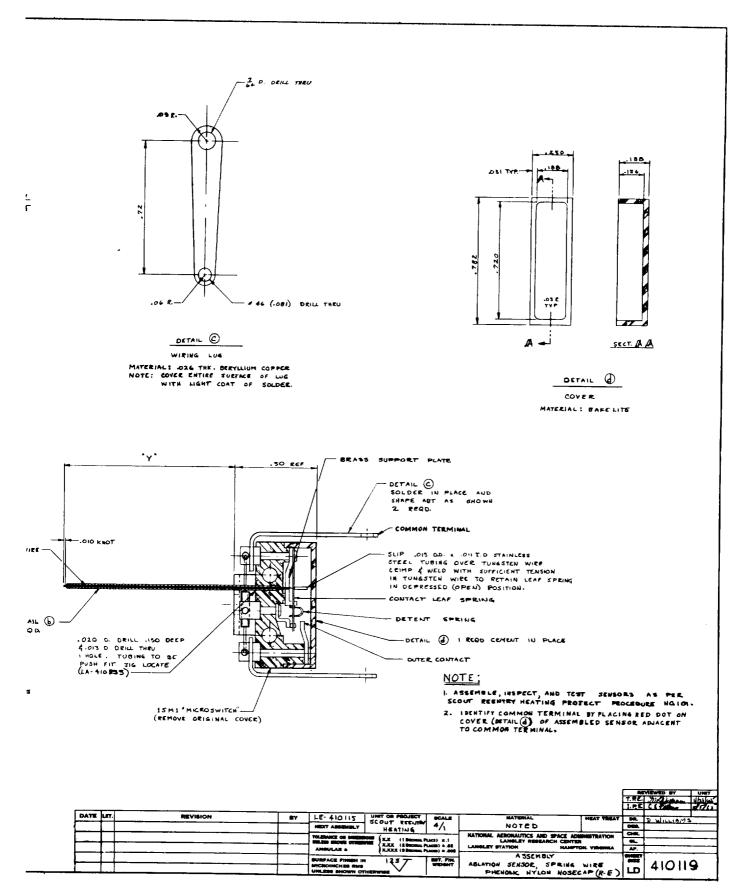


Figure 12. Spring Wire Ablation Sensor Assembly.

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LIGHT PIPE ABLATION SENSOR

PROCEDURE 102

Light Pipe Ablation Sensor Assembly

The light pipe ablation sensor can be fabricated using the procedural steps given below.

- 1. Reference Drawings:
 - (a) Detail assembly (dwg No. LD-410118) figure 15
- 2. Material Required:
 - (a) Ablator plug, drawing detail c
 - (b) Sapphire light pipe, drawing detail a
 - (c) Infrared filter, drawing detail b
 - (d) Diode, Texas Instrument part No. LS-400
 - (e) CIBA 6005, epoxy (Araldite)
 - (f) Versamid 140, reactive resin
 - (g) 0.010 in. ID teflon sleeving
 - (h) 1/64 in. ID teflon sleeving
 - (i) Shielded lead wire, CIMCO type H-28-6736 SGT
- 3. Fabrication and Test Equipment Required:
 - (a) Variac, 0-140 VAC
 - (b) Transformer, 7.5 V filament
 - (c) Tungsten light source, American Optical Co., Model 350
 - (d) Achromatic Condenser, American Optical Co., part No. C235 or C236
 - (e) VOM, Simpson Model 282
 - (f) Precision micrometer
 - (g) Microscope, 20X

Fabrication and Inspection Procedure

Note that all of the following operations are to be carried out in an environment where the relative humidity is controlled at 60 ± 10 percent. The completed sensors shall be stored in this environment. The steps are as follows:

- 1. Record the ablator material control number on the fabrication log, form RE3-1, figure 13.
- 2. Machine the ablation material in accordance with the detail assembly drawing. Record the plug length and the actual diameter measured at the 0.248-in. plug dimension on the fabrication log. Procure serial number for sensor, tag plug, and record number on the fabrication log, form RE3-1.

- 3. Using a filtered, moisture-free air line, direct a stream of air through the 0.187-in. diameter hole from the 0.375-in. diameter end of the ablation plug until the plug is free of dust particles.
- 4. Visually inspect the ablation plug; it shall be free of chips, cracks, and dust.
- 5. Use standard optical procedures to cut and polish the sapphire rod in accordance with dwg No. LD-410118, detail "a". Ultrasonically clean the rods after polishing. Using a microscope, inspect ends of rods for any defects. Measure and record the length of the light pipe on the fabrication log.
- 6. Insert one end of the sapphire rod into the 0.016-in. diameter hole of the ablation plug at the 0.248-in. diameter end. Use a slight rotating motion.
- 7. Place free end of the sapphire rod on a firm surface. Carefully slide the ablation plug down over the rod until the rod is flush with the 0.248-in. diameter surface of the plug.
- 8. Looking at a light source, through the rod from the 0.375-in. diameter end, a round hole 0.016-in. diameter should be visible. If the hole is not round, distortion is present, indicating that either the light pipe is chipped or the light pipe hole is not properly aligned with the 0.082-in. diameter hole. Reject either the ablator plug or the light pipe or both.
- 9. Prepare the infrared filter in accordance with LRC dwg No. LD-410118, detail "b". Measure the diameter and length of the filter and record on the fabrication log. Insert the filter into the ablation plug through the 0.187-in. diameter hole. Make sure the filter is bottomed in the 0.082-in. diameter hole.
- 10. Again, look at a light source, through the filter and the rod to insure that no dust is obstructing the light. The light will have a slightly hazy appearance.

CAUTION

Exercise care while handling the diode; the diode leads are brittle and any flexing may cause the leads to break.

11. Measure the diameter of the diode and record on the fabrication log. In cases where there is excessive paint on the diode body, it may be removed by slight sanding.

NOTE

DO NOT REMOVE THE RED DOT.

- 12. Bottom the diode against the filter in the 0.082-in. diameter hole in the ablator plug. Using the test setup of LRC dwg No. LD-410118, adjust the position of the light pipe assembly until a maximum current indication is noted on the milliammeter. Record the maximum current on the log, form RE3-1. It must be between 18 and 24 milliamperes (ma.). If the maximum current indication is below 18 ma., reject the diode; if above 24 ma., buff the front end of the diode with fine sandpaper sufficiently to make the maximum current fall within the proper range.
- 13. Cut the diode leads and insulate with color-coded teflon sleeving in accordance with LRC dwg No. LD-410118. Solder the 4-foot lengths of lead wires to the diode leads.
- 14. Visually inspect the solder connections for evidence of a poor or cold solder joint. Cover one of the connections with color-coded teflon sleeving.
- 15. Using epoxy resin prepared in accordance with note 3 of LRC dwg No. LD-410118, pot the connection and diode lead wire up to the back end of the detector; then completely fill the cavity behind the diode in the ablator plug, using a fine stick or toothpick to apply the resin. Add small amounts of resin at a time to avoid trapping air bubbles in the plug.

NOTE

Before mixing, the epoxy and resin may be warmed to 115°F, if necessary, to reduce the viscosity and make the mixture more workable.

- 16. After the epoxy has cured for 16 hours at room temperature, recheck the maximum current output of the sensor, using the procedure outlined in step 12, above. Record the maximum current on the log, form RE3-1. If this reading is more than 2 ma. different from the reading taken in step 12, make a note to this effect in the remarks column of form RE3-1.
- 17. Using a Simpson Model 262 volt-ohm-milliammeter (VOM) on the 10K scale, with the positive terminal of the VOM connected to the positive (red) sensor lead, read the diode resistance and record this reading on the log, form RE3-1.
- 18. X-ray the sensor for voids in the potting and kinks in the wire, and attach the X-ray positive to form RE3-1.
- 19. Store the completed sensor in a plastic bag attached to the log, form RE3-1.

20. Periodic current and resistance checks are to be made on the sensor prior to installation in the nosecap and the results recorded on form RE3-1. Whenever resistance is measured, the Model 262 VOM must be used. During installation of the light pipe ablation sensors in the nosecap all pertinent data is to be recorded on the installation log, form RE3-2, figure 14.

REV VEN. INCAL THEOR PRE SNEWLE VIERON V-E45 3845 POSTS POP CURRENT LEVEL
PHP POST LIGHT PIPE ABLATION SENSOR FABRICATION LOG 1551 SOLLORR LNSP DIANETER DIAGRASE CONTRACTOR CO UFNCTH H11 11 H UL AND TER LEN 13 SAPPHIRE ROD PURCHASE , PLATER LENGTH ABLATON PELC ABLACION VATERIAL 13.01 VON TROE. INSTALLED IN PROCEDURE NO 102 SERTAL

Figure 13. Light-Pipe Ablation Sensor Fabrication Log

PORM RESE

T
Post- installation
Pre- installation
Shim thickness
"X"
Depth meas.
Diam. meas.
Hole No.
Diam. meas.
M length measured
L length measured
Mat'1 No.

Figure 14. Light Pipe Ablation Sensor Installation Log.

Form RE3-2

TALE DANGED SE OF EDMS . 745 2:881 .016 D. STOCK

DETAIL @ OPTICAL LIGHT PIPE MATERIAL : FLAME POLICHED WHITE SAPPHIRE ENDS TO BE GROUND FLAT --. 082 500 D.

DETAIL (

INFRA- RED FILTER MATERIAL: CORNING GLASS COLOR STANDARD 1-69
OR CORNING GLASS 4 4600

RED DOT -PHOTO - RESISTIVE DIODE SHALL BE "TEXAS INSTRUMENTS INC." TYPE LS- 400 DETAIL @ --AMERICAN OPTICAL CO, CATALOGUE NO CZ35 OR 236 ACHROMATIC CONDENSOR DETAIL (b) SENSÉE RED LEAD MA DETAIL @-SET VOLTAGE AT THIS POINT TO 75 LAIV SOLDER CON!

TEST SETUP

FIGURE 1.

MERICAN OPTICAL CO. 350 TUNGSTEN LIGHT SOURCE-

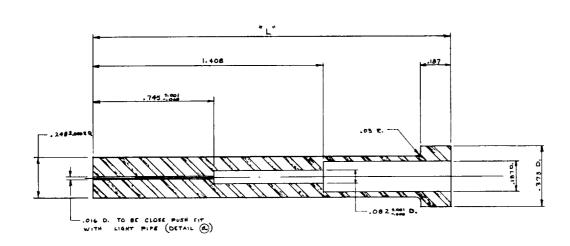
TRANSFORMER

HTV AC

VARIAC-

ı		

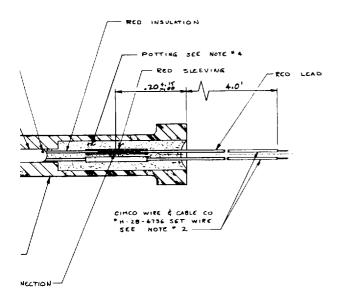
DRAWING NO.	, F.,	TOTAL READ
LD-410118~1	2.200	
- 2	2.150	
-3	2.100	
-4	2.080	
- 5	2.000	
- 6	1.900	
LD-410118 - 7	1.800	



DETAIL @

ABLATOR PLUS

MATERIAL: PHENOLIC NYLON AS PER SCOUT REENTRY HENTING PROTECT PROCEDURE 104



NOTE:

- 1. ASSEMBLE, INSPECT, AND TEST SCUSOR AS PER SCOUT RECUTRY
 HEATING PROTECT PROCEDURE 1072.
 2. PREPARE THE PHOTOSETICTOR FOR INSTALLATION BY COVERING THE
 LEADS WITH TEFLON SLEEVING ATTACH "CIMED WIRE AND
 CABLE CO." H-28-6736 SET WIRE TO THE PHOTODETECTOR LEADS BY
 SOLDERING. COVER BACH JUNCTION WITH INSULATION.
 3. POSITIVE LEAD SHALL BE COLOR CODED AS SHOWN.
- 4. POTTIME SHALL BE "ARALDITE 6005" EPOXY WITH "VECSAMID REACHE RESIN 60% EPOXY & 40% REACTIVE RESIN BY VOLUME. CUES FOR 16 HOURS AT ROOM TEMPERATURE. WITH "VEESAMID 140"
- 5. SCHOOL OUTPUT SHALL BE CHECKED USING SETUP OF FIG. I BEFORE CHECKING SENSORS, CONNECT A SIMPSON 242 VOM TO TRANSFORMER OUTPUT AND ADJUST VARIAC FUR. A METER READING OF 7.5 ± 1 V. MAXIMUM SENSOR CUREBAT OUTPUT HUST BE 18-24 MA. OUTPUT HUST BE CHECKED BEFORE AND AFTER POTTING. OF FIL 1.

										C Carrie	Contract
DATE	LLT.	REVISION	BY	L 410115	SCOUP PRENTRY	4/L	NOTED	HEAT THEAT		D. WILLIAM	1
				TOLINARCE OR DESIGNATION OF THE PERSON OF TH	HEATING SEE XXX (1 December) SEE XXX (2 December)	Lact) ±.1	NATIONAL APPONAUTICS AND SPACE ADM LANGLEY RESEARCH CENTER LANGLEY STATION HAMPIO		E A		
-	H			ANGULAR #		MOT. PML WEDGET	ASSEMBLY	HT PAPE	******	41011	8
				UNLESS SHOWN OT			PHENOLIC NYLON NO	BECAP (RE	<u> </u>		

Figure 15. Optical Light Pipe Sensor Assembly.



T.P.E.I The Land

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THERMOCOUPLE SENSOR

PROCEDURE 103

Thermocouple Sensor Assembly

The procedural steps to fabricate thermocouple sensors are given below.

- 1. Reference Drawings:
 - (a) Thermocouple assembly (dwg No. LD-410117) figure 23.
 - (b) Washer, thermocouple mounting (dwg No. LB-410124) figure 22.
- 2. Material Required:
 - (a) Ablator material, LRC control No.
 - (b) Quartz tubing, 0.010-in. I.D., 0.020-in. O.D.
 - (c) Shell Epon 931
 - (d) Saueresein No. 1
 - (e) Chromel-alumel, B and S 36 gage wire, Thermo Electric Co., Type GC-36-CCT
 - (f) Chromel-alumel, B and S 30 gage wire, Thermo Electric Co., Type GC-30-CCT
 - (g) Washer, mounting
 - (h) Heat shrink tubing, 1/16 inch
 - (i) Heat shrink tubing, 1/8 inch
 - (j) 1/16-in.-diameter copper braided shield
 - (k) Silicone rubber fiberglass sleeving
- 3. Fabrication and Test Equipment Required:
 - (a) VTVM, Hewlett-Packard 412 AR
 - (b) Rubicon resistance bridge
 - (c) Binocular microscope
 - (d) Resistance welder, with weld schedules (figures 19, 20, and 21)
 - (e) Heat gun
 - (f) Wire spacer
 - (g) Wire holding jig

Fabrication and Test Procedures

- 1. Machine ablator material in accordance with the detail as shown on dwg No. LD-410117. Record the LRC control number for the ablator material on the fabrication log, form RE11, figure 16
- 2. Visually inspect the machined plug and make the following observations:

- (a) The plug shall be free of chips, cracks, and dust.
- (b) The outer surface of the plug shall be free of excessive porosity.
- 3. Cut and insert quartz tubing, in accordance with dwg No. LD-410117, into slots at face end of plug and secure with Epon 931. Put in oven to cure.

NOTE

Each time Epon 931 is used, cure at 150° F for 1.5 hours.

- 4. Cut and strip 3-in. length of 36-gage wire, being careful to leave some of the yellow and red insulation for identification.
- 5. Cut 4-foot length of 30-gage wire. Strip 1/4 in. to 3/4 in. on one end according to plug length. Install and shrink a 1-inch piece of small shrink tubing on wire even with point to which wire is stripped. Install 3.75-foot braided shield 1/4 in. from strip point and secure with large shrink tubing. Slide fiberglass sleeving over cable and even with strip point.
- 6. Weld 3-inch length of 36-gage wire to prepared end of 30-gage wire, observing color of insulation to ensure that like wires are welded together.
- 7. Remove remainder of insulation from 36-gage wire and slide into rear of quartz on plug. Pull wires through quartz. Make sure that cable is tight against rear of plug, and secure wire in this position with clip.
- 8. Dress wires into slots on plug and fill to surface of plug with Epon 931. Put in oven and cure.
- 9. Remove thermocouple assembly from oven, and remove clip. Fill any voids and bond cap on plug with Epon 931. Make certain that cap is square with plug and cure in oven.
- 10. Prepare and make thermocouple weld at front end of plug.
 Dress thermocouple to proper "S" formation. Insert Saueresein
 No. 1 into face end of quartz about 1/8 in. Cure in oven for
 15 minutes at 150° F.
- 11. Using the Rubicon resistance bridge, measure and record on form RE11, figure 16, forward and reverse resistances of thermocouple.
- 12. Using VTVM, check thermocouple weld for proper wiring by heating with soldering iron, and record results on form RE11.

NOTE

Use low temperature and extreme care to avoid damage to ablation material.

- 13. Measure and record physical dimensions of plug on form RE11. Measure at several points to ensure that measurements are constant.
- 14. Attach protective cap and washer shim to cable, and store assembly in a clean envelope with copy of form RE11.
- 15. The appropriate data must be recorded on form RE12, figure 17, and after installation in the nosecap the thermocouple data should be entered on the location log, form RE1, figure 18.

	THERMOCOUPLE FABRICATION LOG	
Serial No.	Drawing No. 410117-	Date
DIMENSIONS Length - P Diameter - Initia Length - L Length - M Diameter - Final Washer shim thick		CONTROL NUMBERS LRC ablator batch control number T/C wire control number 30 gage T/C wire control number 36 gage
POLARITY Chromel (yellow) Alumel (red) - RESISTANCE Forward Reverse Chromel leakage Alumel leakage	+ Initial Final	LOCATION Install in Hole number

Form RE11

Figure 16. Thermocouple Fabrication Log

THERMOCOUPLE PLUG AND CAP

Ablator Material No.

Work Order No.

	No. mach.	Check quantity	Remarks
Drawing LD-410117 - 1		t de la constitución de la const	
- 2			
- 3			
- 4			
- 5			
- 6			
- 7			
- 8			
- 9			
- 10			
- 11			
- 12			
- 13			
- 14			
- 1 5			
- 16			
- 17			
	7	Total No. Plugs	
	7	Cotal No. Caps	

Form RE12

Figure 17. Thermocouple Log

		-	Alumel leakage								
		nal electrical resistance	Chromel leakage								
Date		Final e	Post								
			Pre								
		Washer	Shim thickness								
500		^	"X"								
MOCOUPLE LOCATION LOG		Assembly (Mat'l No.	Depth meas.								
RMOCOUPLE LO	ON THE		Diam. meas.								
ERMOCC	WITCOU .		Hole No.								
THERN									<u> </u>	Diam. meas.	
		(Mat'l No.	M length measured								
			L length measured								
		Thermocouple	Serial number								

Figure 18. Thermocouple Location Log

Form RE1

PRESSURE CONTROL FOR THIS TYPE WELDER ONLY)
(IN TERMS OF HALF-TURN DIVISIONS OF CALIBRATED

FLECTRODE PRESSURE

Isostrength Chart, Chromel to Chromel

Figure 19.

ENERGY (WATT/SEC) (1/15 DIVISIONS)

1											מ. ַ ך
	6C 1032	3 X	×	×	×	×	×	×	×		$\frac{30}{2w/s}$
)26(×	×	×	×	×	×	×		26
	, 10	X	×	×	×	×	×	×	×		28
	EQUIPMENT USED WELDMATIC—MODEL 1026C NASA 96573 WELDING HEAD—MODEL 10		×	×	×	×	×	×	×		27
	USED MOD	X	×	×	×	×	×	×	×		26
	NT IC- 573	- 1	×	×	×	×	×	×	×		25
	EQUIPMENT WELDMATIC NASA 9657	X	×	×	×	×	×	×	×		24
	QUI ELD ASA	j ×	: ×	×	×	×	×	×	×		23
	M	[≟]	: ×	×	×	×	×	×	×		22
		×	: ×	×	×	×	×	×	×		21
		×	: ×	×	×	×	×	×	×		20
	65	×	: ×	×	×	×	×	×	×		19
	4/27/65	×	: ×	×	×	×	×	×	×		18
		×	: ×	×	×	×	×	×	×		17
	DATE (ELD)	×	* ×	*	*	*	×	×	×		16
	W.	\ \	(*	*	Ü	G	*	×	×		15 1w/s
	ULE - DATE TO (LAP WELD)		+	ტ	ß	ڻ ت	*	×	×		14
		 	‹ *	*	_ 5	*	*	×	×		13
	D SCHEI FOR ALUMEL		4 *	*	*	*	×	×	×		12]
	FO AL	\	4 ×	 	*	*	×	×	×		11 1
	WE]	,	< ×	: ×	*	*	×	×	×		10 1
		 	< ×	: ×	×	×	×	×	×		9 1
		,	< ×	: ×	×	×	×	×	×		∞
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	USED No W		`		×	×	×	×	×		4
	(500) **	<u>.</u>	` . < ×		×	×	×	×	×		က
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					~ ×	×	×	×	×		-
										008795488-	_ن
		c c	31 22	30	29	28	27	26	25	01 00 87 94 10 10	•

Isostrength Chart, Alumel to Alumel

Figure 20.

ENERGY (WATT/SEC) (1/15 DIVISIONS)

DEESSURE CONTROL FOR THIS TYPE WELDER ONLY)
(IN TERMS OF HALF-TURN DIVISIONS OF CALIBRATED ELECTRODE PRESSURE

•													
6C 1032	×	×	×	×	×	×	×	×	×	×	×		30 $2w/s$
01 1	×	×	×	×	×	×	×	×	×	×	×	•	29
T USED C-MODEL 10 73 HEAD-MODEL	×	×	×	×	×	×	×	×	×	×	×	,	28
DEL MO	×	×	×	×	×	×	×	×	×	×	×		27
USED—MODEL	×	×	×	×	×	×	×	×	×	×	×		26
(TT C C S 7 3 HE	×	×	×	×	×	×	×	×	×	×	×		25
EQUIPMENT WELDMATIC- NASA 96573 WELDING HE	×	×	×	×	×	×	×	×	×	×	×		24
EQUIPME WELDMAT NASA 96 WELDING	×	×	×	×	×	×	×	×	×	×	×		23
	×	×	×	×	×	×	×	×	×	×	×		22
	×	×	×	×	×	×	×	×	×	×	×		21
	×	×	×	×	×	×	×	×	×	×	×		20
က္	×	×	×	×	×	×	×	×	×	×	×		19
4/21/65	×	×	×	×	×	*	×	×	×	×	×		18
4/2	×	×	×	*	*	*	*	*	×	×	×		17
DATE VELD)	×	×	×	*	ტ	ŗ	ტ	*	×	×	×		16
- DA	×	×	×	ტ	ტ	ß	ტ	Ö	×	×	×		15 1w/s
<u> </u>	×	×	×	Ö	G	IJ	G	ŋ	*	×	×		14
	×	×	×	*	ტ	ტ	G	ტ	×	×	×		13
D SCHED FOR CHROMEL ALUMEL	×	×	×	*	*	Ö	G	*	×	×	×		12
	×	×	×	*	*	G	*	*	×	×	×		11
WELD FC 36 CF 36 AI	×	×	×	×	*	*	*	*	×	×	×		10
	×	×	×	×	×	*	*	×	×	×	×		6
	×	×	×	×	×	×	×	×	×	×	×		œ
INS Ike d	×	×	×	×	×	×	×	×	×	×	×		2
IMENS)	×	×	×	×	×	×	×	×	×	×	×		9
SPECIM USED) No Weld Weld Br Good We	×	×	×	×	×	×	×	×	×	×	×		က
Ō	×	×	×	×	×	×	×	×	×	×	×		4
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	×	×	×	×	×	×	×	×	×	×	×		H
	32	31	30	29	28	27	26	25	24	23	22	0087964604	- -

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CYPIBEATED PRESSURE CONTROL FOR THIS
(IN TERMS OF HALF-TURN DIVISIONS OF
ELECTRODE PRESSURE

43

21. Isostrength Chart, Chromel to Alumel

ENERGY (WATT/SEC) (1/15 DIVISIONS)

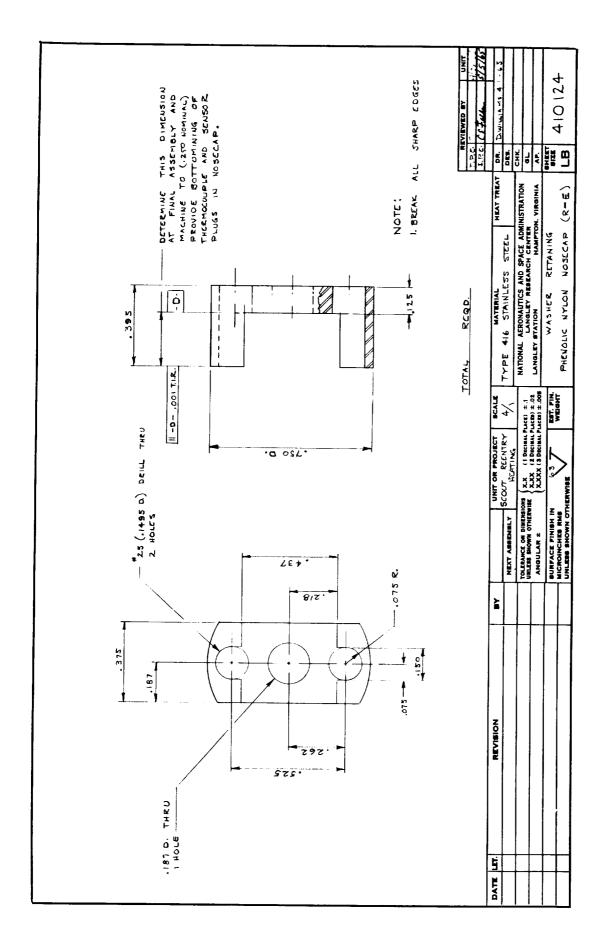


Figure 22. Phenolic Nylon Nosecap Retaining Washer

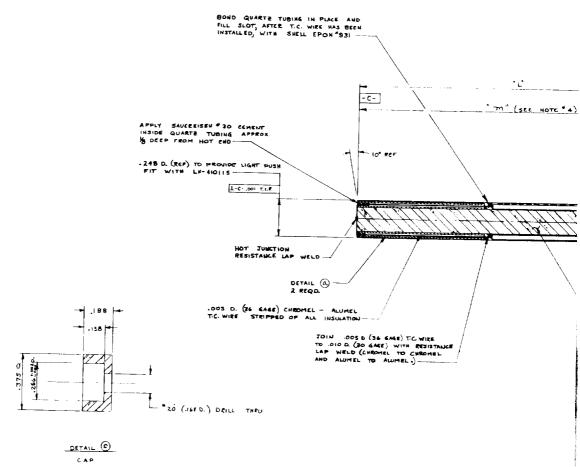


DETAIL @

QUARTE TUBING

MATERIAL: .020 D.D. s. .010 I.D. QUARTE

TUBING.



MATERIAL: PHENDIC NYLON AS PER SCOUT
REENTRY HEATING PROJECT PROCEDURE 104

1		

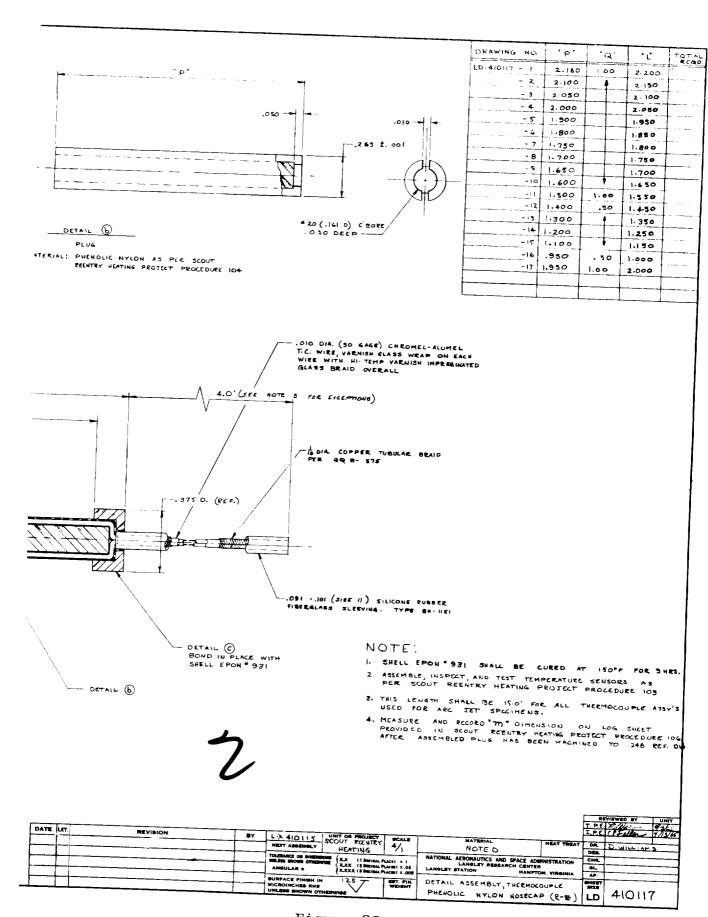


Figure 23. Thermocouple Detail Assembly.

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MOLDING ABLATOR

PROCEDURE 104

Ablator, Phenolic Nylon Nosecap

Molding of the ablator material was accomplished using the following steps.

- 1. Reference Drawings and Sketches:
 - (a) Ablator contour (LRC Dwg No. LC-410120) figure 28
 - (b) Nose cap mold LRC Dwg No. LX-409155
 - (c) Thermocouple sensing probe LRC Dwg No. LB-410318
 - (d) Sketch No. 1, figure 27, mold thermocouple and pressure transducer locations

2. Materials Required:

- (a) Powdered 66 Nylon Dupont Zytel 103, MP and DS Control No. L64-6D.615.L261968/C
- (b) Powdered phenolic resin, Union Carbide Corporation's BRP-5549, MP and DS Control No. U2-19D.576.L60248/C
- (c) Phenolic microballoons, Union Carbide Corporation's BJO-0930, MP and DS Control No. U2-19D.620.L1986/C.
- (d) Vinyl tape, Federal Stock No. 8135-634-3330
- (e) TF freon precision cleaning agent, E. I. Dupont
- (f) Methyl ethyl ketone solvent, Federal Stock No. 6810-281-2762
- (g) Miller-Stephenson MS-122 parting agent
- (h) Iron-constantan thermocouple wire, certified calibration
- (i) Chromel-alumel thermocouple wire, certified calibration
- (j) Liquid argon gas
- (k) Ram Chemical Company's Plastilease 344
- (1) Copies of purchase specifications and manufacturer's certifications of materials attached

3. Equipment Required:

- (a) Processor, Patterson-Kelly, 5 cu ft capacity
- (b) Processor, Patterson-Kelly, 1 cu ft capacity
- (c) Blackstone ultrasonic degreaser, Model VR-20-3
- (d) Shadowgraph scale, Model 4112-HB
- (e) Barber-Coleman pressure transducer system, composed of pressure recorder console and 6 calibrated transducers, 0 10,000 psi, pressure calibration chart attached
- (f) Press, Oliver, 500-ton capacity
- (g) Nosecap mold
- (h) Thermocouple sensing probe
- (i) Millimeter vacuum gage

- (j) 200 C.F.M. vacuum pump
- (k) Honeywell-Brown recorder, 0 600°F, iron-constantan. Certified calibration No. 30 and 36 gage I.C. thermocouple wire.
- (1) Honeywell-Brown recorder, 0 1000° F, chromel-alumel. Certified calibration No. 30 gage C.A. thermocouple wire.
- (m) Inch-pound torque wrench
- (n) Oven, air circulating, 0 600° F, program-controlled
- (o) Oven retort, stainless steel
- (p) Argon flow meter
- (q) Grain sampler, Dean Gamet Mfg. Co.

Raw Materials Sampling Procedure

- 1. Presampling of each raw ingredient container for particle size distribution study is performed in the following manner:
 - (a) Identify each raw material container of nylon, microballoons, and phenolic resin with a letter designation in the order listed below.
 - 1. Three nylon containers containers A, B, and C.
 - Four microballoon containers containers D, E, F, and G.
 - 3. One phenolic resin container container H.
 - (b) Insert a probe grain sampler vertically in the storage drum center while sampler is in a closed position.
 - (c) Tilt the storage drum as far as possible without disturbing the material, having the sampler openings facing upward.
 - (d) Open the sampler to permit the material to fill the six sampler cavities. Close the sampler, right the drum, and remove the sampler from the drum.
 - (e) Open the sampler and remove the material samples. Package the material in a polyethylene bag, and identify with a sampler zone number and drum letter designation. Identify each bag as to material that has not been processed.
 - (f) Empty the contents of the storage drum into the 5-cu ft blender and mix for 15 ± 2 minutes.
 - (g) Empty mixed material from blender back into original storage container, and sample as directed in steps 1(a) through 1(d). Identify the samples as having been mixed as directed in step 1(f) above.
- 2. The following procedure is used to sample the individual raw materials, nylon, phenolic resin, and phenolic microballoons, for evaluation by Hughes Aircraft Co. on Contract No. NAS2-2739. Samples are taken of each ingredient prior to processing each individual raw material for molding. Determine the level to

which the material storage drum is filled, as received from the manufacturer. Mark a pencil line on the outside of the drum at this level. Divide and number the drum into eight equal zones from top to bottom, starting with zone No. 1 at the top. For example, container A, B, C, etc., and individual container zone A1, A2, A3, etc.

- 3. Weigh out the proper amount of raw material, in accordance with 1(a), 2(a), and 3(a) on the shadowgraph scale, into a clean polyethylene container.
- 4. Vacuum out the P-K blender mix hopper and clean with a clean cloth moistened with TF freon.
- 5. Load the blender with the individual raw material being sampled and mix for 10 ± 2 minutes at 8 ± 1 rpm hopper speed.
- 6. Weigh out one-half pound of mixed material on shadowgraph scale into a polyethylene bag. Heat-seal bag opening. Repackage unused raw material in polyethylene container, for further processing. Seal lid of container with vinyl tape, Federal Stock No. 8135-634-3330.
- 7. Assign a number to the sample, using the numbering sequence given in figure 26, and identify the bag with this number. Record this number on, and complete three copies of, the sampling log sheet, form RE7, figure 25. Affix one copy of sampling log sheet to bagged sample with masking tape, attach second copy to this procedure, and retain third copy for MP and DS Files.
- 8. Package sample in a one gallon, wide-mouth metal container for shipment. Where volume of one-half pound sample is too large to fit in a gallon container, divide the sample into a suitable number of smaller bags. Identify each bag with sample number.
- 9. Initiate LRC Shipping Order, Form P.C. 36F099. Ship to:

Mr. L. B. Keller Hughes Aircraft Company Bldg. 32, Mail Station H-164 Culver City, California

Material Formulation and Compounding

The material formulation is composed of the following percentages by weight of nylon, phenolic resin, and phenolic microballoons:

40-percent powdered nylon, Zytel 103 25-percent phenolic resin, BRP-5549 35-percent phenolic microballoons, BJO-0930

- 1. Preprocessing of Nylon
 - (a) Degrease polyethylene material container in freon. Refer to paragraph 2 under Raw Materials Sampling Procedure for zone identification of raw material storage drum. Weigh out 2,650 grams of nylon in the container on Shadowgraph scales.
 - (b) Take from this weighing a sample of approximately 60 grams. Package the sample in a heat-sealed polyethylene bag. Assign a number to the sample. Identify it and ship to chemical laboratory for moisture content analysis. Record the following data:

Record sample No.:______

Record moisture content: _____percent.

Record information on form RE6, figure 24

- (c) Sample weighing ad directed in paragraphs 4 through 9 under Raw Materials Sampling Procedure.
- (d) Secure hopper lids and dry as follows:

180 ± 5 minutes at 200 ± 5 F

 29 ± 1 inches of mercury

 5 ± 1 rpm hopper speed

Record mix time: ____minutes.

Record hopper temp: ____ F.

Record hopper rpm setting: ___ rpm.

Record vacuum: ____ in. mercury.

(e) Remove dried material from blender and place in polyethylene container. Take a sample as directed in step 1(b). Use same sample number with a letter suffix to show that sample has been dried.

Record sample No.:

Record moisture content: ____ percent.

Record information on form RE6.

(f)	Reweigh nylon on shadowgraph scale and adjust weight to $2,060 \pm 5$ grams for correct percentage of total formulation weight.
	weight.

Record weight: ____ grams.

Seal lid of polyethylene container with vinyl tape, Federal Stock No. 8135-634-3330.

- (g) Mark on the container with a brush pen the total material weight, the time of day, and the date. Predried material shall be compounded into a batch formulation within 48 hours.
- (h) Record weight of nylon, reference step 1(b), on fabrication log sheet, form RE6.

2. Preprocessing of Phenolic Resin

- (a) Degrease polyethylene material container in Blackstone degreaser with freon. Refer to paragraph 2 under Raw Materials Sampling Procedure for zone identification of raw material storage drum. Weigh out 1,830 grams of phenolic resin in the container on the shadowgraph scales.
- (b) Take from the weighing a sample of approximately 60 grams. Package the sample in a heat-sealed polyethylene bag. Assign a number to the sample. Identify it and ship to chemical laboratory for moisture content analysis.

Record No.: ____

Record moisture content: ____ percent.

Record information on form RE6.

- (c) Sample weighing as directed in paragraphs 4 through 9 under Raw Materials Sampling Procedure.
- (d) Remove material from blender and reweigh on shadowgraph scales. Adjust weight to 1,287 ±5 grams for correct percentage of total formulation weight.

Record weight: ____ grams

Seal lid of polyethylene container with vinyl tape, Federal Stock No. 8135-634-3330.

(e) Record weight of phenolic resin on fabrication log sheet, form RE6.

3. Preprocessing of Microballoons

(a) Degrease polyethylene material container in Blackstone degreaser with freon. Refer to paragraph 2 under Raw Materials Sampling Procedure for zone identification of raw material storage drum. Weigh out 2,400 grams of microballoons in the container on shadowgraph scales.

(b)	Take from this weighing a sample of approximately 60 grams. Package the sample in a heat-sealed polyethylene bag. Assign a number of the sample. Identify it and ship to chemical laboratory for moisture content.
	Record Sample No.:
	Record moisture content: percent.
	Record information on Form RE6.
(c) (d)	Sample weighing as directed in paragraphs 4 through 9 under Raw Materials Sampling Procedure. Secure hopper lids and dry as follows:
	180 ± 5 minutes at 200 $\pm 5^{\circ}$ F.
	29 ±1 inches of mercury.
	5 ±1 rpm hopper speed.
	Record mix time: minutes.
	Record hopper temp: F.
	Record hopper rpm setting:rpm (setting No. 2).
	Record vacuum: in. mercury.
(e)	Remove dried material from blender and place in polyeth- lene container. Take a sample as directed in step 3(b). Use same sample number as assigned in step 3(b) and assign a letter suffix to indicate that sample has been dried.
	Record sample No.:
	Record moisture content: percent.
	Record information on form RE6.
(f)	Reweigh microballoons on shadowgraph scales, and adjust weight to 1,803 ± 5 grams for correct percentage of total formulation weight.
	Record weight: grams.
	Seal lid of polyethylene container with vinyl tape, Federal Stock No. 8135-634-3330.
(g)	Mark on the container with a brush pen the total material weight, the time of day, and the date. Predried material shall be compounded into a batch formulation within 48 hours.

(h)	Record weight of microballoons, reference step 3(b), on fabrication log sheet, form RE6.
Comp	osition Batch Formulation
(a)	Record the formulation weights of each raw material, and assign a batch control number to the formulation
	25 percent phenolic resin: grams
	40 percent nylon: grams
	35 Percent microballoons: grams
	Batch number:
	Record information on form RE6.
(b)	Load the hopper with predried microballoons by sifting them through a No. 20, U.S. standard mesh screen. Degrease screen in Blackstone degreaser with freon before using.
(c)	Mix for 5 ± 1 minutes at room temperature using 14 ± 1 rpm hopper speed, without vacuum.
	Record mix time: minutes.
	Record hopper rpm setting:rpm.
(d)	Load hopper with predried nylon by sifting through No. 20, U.S. standard mesh screen. Mix for 2 minutes with intensity bar after addition of all nylon.
(e)	Mix nylon and microballoons together for 10 ± 2 minutes at room temperature and 14 ± 1 rpm hopper speed, without vacuum.
	Record mix time: minutes.
	Record hopper rpm setting:rpm
(f) (g)	Visually inspect mix for improper mixing or lumping. Load the hopper with phenolic resin by sifting through a No. 20, U.S. standard mesh screen. Mix for 2 minutes with

4.

intensity bar after addition of all phenolic resin.

(h) Mix nylon, microballoons, and phenolic resin together for 10 ± 2 minutes at room temperature and 14 ± 1 rpm hopper speed, without vacuum. Visually inspect for proper mixing.

Record mix time: ____ minutes.

Record hopper rpm setting:__rpm.

(i) Remove a one-half pound sample of material and heat-seal in a polyethylene bag. Identify bag with batch number.

(j) Package and ship in accordance with paragraphs 8 and 9 under Raw Materials Sampling Procedure.

(k) Empty formulated batch from blender into a suitable size preweighed polyethylene bag. Reweigh batch on shadowgraph scales, and adjust weight to 4,805 ±100 grams for correct mold charge weight.

Record weight: ____ grams

- (1) Seal neck of polythylene bag by twisting several times and folding it back on itself. Secure with masking tape and place bag in polyethylene container. Seal lid of polyethylene container with vinyl tape, Federal Stock No. 8135—634-3330. Mark with a brush pen on the side of the container the time of day, the date, and the molding composition weight and batch number. Store at room temperature.
- (m) Formulated batch must not be stored for more than 72 hours prior to molding.

Mold Assembly and Instrumentation

- 1. Refer to sketch No. 1 (figure 27) of this procedure for proper location and numbering sequence of all thermocouples and pressure transducers.
- 2. Position two steel adapter blocks on bottom press platen. Position two silicone laminate insulating plates, one on each block, on top of steel adapter blocks. Position and align heating platen on top of insulating plates, and dog down with tie rod studs. Align mold base plate in the molding press on the lower heating platen, and secure with machine screws.
- 3. Using an ohmmeter, check electrical continuity of thermocouples No. 7 and 8, which are welded to the inside bottom face of mold plunger.
- 4. Connect water lines and fittings to two calibrated transducers, and install the transducers in the mold plunger at transducer locations No. 2 and 3. Torque each transducer to 50 in. -1b. Record the transducer number and serial number relative to its location. Reference should be made to the transducer calibration chart.

Location No. 2 - Transducer No.____, Serial No.____ Location No. 3 - Transducer No.____, Serial No.____

- 5. Position the **3**.4-in. thick silicone laminate insulation plate and the 2-in. thick steel adapter plate on top of mold plunger. Secure to plunger with Allen head machine screws.
- 6. Center the mold plunger in the molding press on top of the mold base, using the base plate "0" ring groove as a reference.
- 7. Thread the transducer leads, the water lines, and the thermocouple leads through the opening in the top press platen.

- 8. Raise the mold plunger into place by slowly closing the molding press. Fasten it to the top platen with machine screws.
- 9. Lower the press and remove the mold base plate from the molding press.
- 10. Install the thermocouple temperature probe in the mold base plate. Check the electrical continuity of thermocouples No. 4, 5, and 6 with an ohmmeter.
- 11. Align the mold base plate in the molding press on the lower heating platen. Fasten to heating platen with Allen head machine screws. Install a calibrated pressure transducer in the mold base plate at transducer location No. 1. Torque to 50 in.—lb. Connect the water lines and fittings to the transducer. Record the transducer number and serial number.

Location No. 1 - Transducer No. ___, Serial No. ___

- 12. Using a clean cloth moistened with methyl ethyl ketone, solvent-clean the mold base plate, male plunger, and female cavity in all areas that will come in contact with the molding compound. Repeat cleaning operation using TF freon solvent.
- 13. Apply Ram Chemical Company's Plastilease 334 wax and rub out. Spray two thin, uniform coatings of Miller-Stephenson MS-122 parting agent on cleaned mold areas, wiping off excess between first and second coat.
- 14. Install silicone "0" ring in mold base plate "0" ring groove. Install silicone "0" ring on outside diameter of mold plunger. Push "0" ring to top of plunger.
- 15. Position and align mold female cavity on mold base plate in base plate index flange. Check alignment of female cavity with mold plunger by closing press and shifting female cavity as needed. Fasten female mold cavity to press platen with two sets of studs and dogs.
- 16. Connect thermocouple leads No. 1 through 12 to the correspondingly numbered channels of the Honeywell-Brown temperature recording instrument. As a check for correct operation, turn the instrument on and record the ambient temperature of each thermocouple.

NOTE

The Honeywell-Brown temperature recording instrument is automatically controlled so that it will make a temperature record at 11.5-minute intervals. The time required to make a single plot is 30 seconds. It

can also be manually controlled to print 100 percent of time by turning off clock control switch and turning on chart drive switch.

- 17. Connect the inlet water lines of all pressure transducers to the water source valve. Place the outlet water lines in the end of the main water line drain hose. Turn on the water and check each transducer outlet hose for the proper amount of water flow.
- 18. Fasten the electrical pressure leads coming from the pressure transducers at locations No. 1, 2, and 3 to the correspondingly numbered channels of the Barber-Coleman pressure recording instrument. Turn the instrument on and run through a trace of each transducer. The trace of each should indicate 0 pressure. Turn the instrument off.
- 19. Make up all steam line connections to the mold bottom heating platen, male plunger, and mold female cavity.

Molding Procedure

- 1. Cut out one 12-inch diameter disc of 1/8-inch thick fiberfrax (aluminum-silicate) felt. Cut out three 12-inch diameter discs of 15-mil square weave fiberglass cloth. Cut out a suitable size hole in the correct location so that the thermocouple probe can protrude through.
- 2. Position the four layers of the above material on the mold base plates so that the fiberglass cloth is on the bottom. These layers constitute the bottom volatile sink.
- 3. Remove the formulated molding compound from the storage room. Unseal the polyethylene container and remove bag from the container. Assign an ablator molding number to the composition, and record.

Ablator Molding No. ____

- 4. Remove the tape from the neck of the polyethylene bag. Holding the neck closed (folded on itself) with one hand and the weight of the bag with the other hand, insert the bag, neck end down, in the mold cavity until the bag rests on the mold base plate.
- 5. Release the neck of the bag and gently withdraw it from the mold cavity by grasping it at the bottom with both hands. Gently shake the bag during the withdrawing operation to ensure complete emptying.

6. Record the shop work area temperature and relative humidity during the loading operation.

Temperature:		F		
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Relative humidity: ____ percent.

- 7. Using a small straightedge 4 to 6 inches long, grade the top of the molding composition level.
- 8. Cut the volatile sink material as directed in step 1 above, omitting hole in approximate center, and position the material on top of the leveled composition so that the fiberfrax felt is in contact with the molding composition.
- 9. The following steps 10 through 18 are a specialized technique developed for, and adapted to, the existing LRC molding equipment. To meet the acceptance criteria as to bulk and unit density variation of ablator moldings, it is necessary to control the unit density at the top and bottom. This is accomplished by compressing the molding composition 7/8 inch beyond its normal thickness of 4-1/2 inches at room temperature. The composition is allowed to recover under the dead weight of the top press platen and male plunger (2,011 lb) to 4-1/2 inches.
- 10. Measure to the nearest 1/4 inch the distance from the top of the volatile sink to the top of the female mold cavity, using a 24-inch scale and square head. Add 1-1/2 inches to this measurement, and measure up from the bottom of the mold plunger using this dimension. Using a crayon pencil, mark a line on the male plunger (reference line "A") to represent this dimension.
- 11. Energize the molding press hydraulic pump motor. Set the control index on the press control on COMPRESSION. Lift the arm on the limit switch marked LS-4 SLOW APPROACH with left hand.
- 12. With the right hand push in the CYCLE START button. As press starts closing on slow approach, release the limit switch arm and place right hand on CONTROL INDEX switch. When the top surface of the female cavity reaches reference mark "A" on the mold plunger, turn the CONTROL INDEX switch to the MANUAL position. Press travel will cease and hold at this reference mark. Turn the press pump motor off.
- 13. Connect one vacuum line from vacuum pump to top of mold female cavity and one vacuum line to mold base plate. Refer to figure 16. Slide the "0" ring around the mold plunger down into the "0" ring groove at top of mold female cavity. Close both vacuum valves on vacuum manifold.
- 14. Turn on the vacuum pump. Open the vacuum valve which controls the vacuum line to the mold base plate. Evacuate the mold

cavity through this line at a rate of 38 ± 5 millimeters mercury per minute. Evacuate cavity to $5\pm \frac{0}{5}$ millimeters mercury. Open vacuum line to top of female cavity. Evacuate cavity through both lines for 40 ± 5 minutes. Record maximum vacuum pressure and total time evacuated.

Maximum vacuum pressure:	mm.
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Total time: minute

- 15. Position two steel stop shims, $1 \times 6-1/8 \times 8$ inches, on top surface of female mold cavity, one on each side, $180^{\rm O}$ apart. Use the 6-1/8 inch dimesion as the shim height. The shims should be placed in such a manner that when the press closes they will land on the mold plunger adapter plate.
- 16. Turn on the Barber-Coleman recording instrument to record pressure. Record on the recording chart the start of stress relief cycle, ablator molding number, date, and time of day. To conform to the processing criteria of this procedure, one of the three pressure transducers must be recording properly the pressure on the material composition during molding cycle only. Energize the press hydraulic pump motor. Position the CONTROL INDEX switch on the press control panel to COMPRESSION. With left hand, lift arm of limit switch marked LS-4 SLOW APPROACH. Depress CYCLE START button with right hand. As press closes on slow approach, maintain a uniform closing speed by increasing the clamp pressure.
- 17. Immediately after shim stops land on plunger adapter plate, back off the clamp pressure to the minimum available pressure, which is approximately 100 tons. Turn CONTROL INDEX switch to MANUAL. Start opening the press with the CLAMP INCH-DOWN BUTTON. Stop when daylight appears between the top molding press bolsters and the insulation plate. Turn off the hydraulic pump motor. Hold this position with no more than 3/8-inch maximum daylight showing while the molding compound recovers 7/8 inch. Record the length of time required for molding compound to recover, using a stop watch.

Time to recover: ___ min ___ sec

18. Position two steel shims 7/8-inch thick, one each on the 6-1/8-inch shim stops. Energize hydraulic pump motor and reclose press on shim stops as in step 16 using 90- to 100-ton clamp pressure.

Cure Cycle

- 1. Mark a pencil line on the Barber-Coleman pressure recording chart and the Honeywell-Brown temperature recording chart and label as START OF THE CURE CYCLE. Record on the Honeywell-Brown recording chart the ablator molding number, date, and time of day. Turn on the chart drive switch for full time recording.
- 2. Close the steam valve to the lower heating platen.
- 3. Open the steam valve to the mold male plunger and female cavity. Set the steam pressure at 40 lb, and heat-mold for 30 ± 5 minutes at this pressure.
- 4. After 30 minutes raise the steam pressure on the mold male plunger to 60 lb and on the mold female cavity to 75 lb. Heat at this new setting for 2 hours ± 5 minutes. After 2 hours turn on the steam to the bottom heating platen. Adjust the top and bottom steam pressure regulator valves to raise the mold temperature to $335 \pm 5^{\circ}$ F, which is controlled by thermocouples No. 2 and No. 3. In making this adjustment, set the top steam pressure regulator valve 15 ± 4 lb below the setting of the bottom regulator valve. To conform to the process criteria of this procedure, only one of these thermocouples must be recording at all times during the cure cycle.
- 5. After balancing out the mold temperature to 335 $\pm 10^{\circ}$ F, set up timer of Honeywell-Brown recorder for 4 percent time on. Turn off manual chart drive control switch and turn on timer control switch.
- 6. Heat the molding composition at 315 ± 0^{100} F using any one of the three probe thermocouples (No. 4, 5, and 6) as the temperature control point. To conform to the process criteria of this procedure, only one of these thermocouples must be recording at all times during the cure cycle. Record the time required to reach the cure temperature based on the starting time and the temperature point at which the cure time starts.

Temperature point: ____ F. ___

Time required to reach cure temp: ____ hr ___ min.

7. Cure at 315 ± 0 F for 3 hours \pm 10 minutes. Mark on the temperature recording chart the point where the curing time starts and ends, and record here the total curing time.

Curing time: hr min.

8. At the end of cure time, turn off steam and vacuum to mold. Return the CONTROL INDEX SWITCH to MANUAL. Shut off the molding

press hydraulic pump motor. Turn off the Barber-Coleman pressure recording instrument. Do not turn off the Honeywell-Brown temperature recording instrument.

- 9. Cool the molded ablator in the mold to 275 \pm^0_{10} F, as indicated by probe thermocouple control point, before removing. Turn off the Honeywell-Brown temperature recorder. Turn off water to transducers.
- 10. To remove the molded ablator from the mold, proceed as follows:
 - (a) Energize the hydraulic pump motor on the press. Lower the press until the mold plunger is 1 to 2 inches from becoming disengaged from the mold female cavity.
 - (b) Remove vacuum lines and vacuum port nipple from female mold.
 - (c) Disconnect copper steam lines from female mold, and remove holdown machine screws.
 - (d) Push female support carriage into place.
 - (e) Open press until female mold engages in support carriage and bottom of female mold is 2 inches above mold base plate.
 - (f) Lift ablator molding off mold base plate back into female mold cavity, and support it at this position.
 - (g) Open press to full opening and shut off hydraulic pump motor.
 - (h) Roll carriage out of molding press and remove ablator molding from mold.
- 11. Place ablator molding in an insulated container as soon as it is removed from the mold, and allow it to cool for $10~\pm 2~hours$. The insulated container shall be at room temperature.
- 12. Remove the volatile sink material from top and bottom of ablator molding. Identify the molding as Scout RE, with formulation batch number and molding number. Affix identification tag of embossed aluminum pressure-sensitive tape to the diameter of the cake.

Example - Scout RE.FB-1.AM-1 Formulation Batch - FB Ablator Molding - AM

- 13. Remove from the Barber-Coleman and Honeywell-Brown recorders the chart paper of the cure cycle. Draw a single graphical plot of the time, temperature pressure curves. Identify the graph as form RE8 and record the date, job order, formulation batch number, and molding number. Attach to form RE8 (figure 39) of this procedure recording charts and graph.
- 14. Machine 1/8 inch from top and bottom of the molded cake, holding the faces parallel within 0.003 inch. Machine the cake dry.

Post Mold Density Determination

- 1. Refer to form RE6 and record all pertinent calculations as developed. Remove the identification tag.
- 2. Weigh the ablator molding to the nearest 0.001 pound.
- 3. Divide the ablator molding on bottom face into six equal spaces, marking the division points with a soft lead pencil. Connect the diagonally opposite points with a line drawn through the center. Measure in from the diameter, 1 inch from outer edge on each line.
- 4. With a micrometer measure the ablator thickness at the six location points to the nearest 0.0001 inch. Calculate the thickness of the ablator molding as an average of these measurements.
- 5. Measure with a micrometer the diameter of the ablator molding to the nearest 0.0001 inch. Make these diameter measurements at three different points, and calculate the ablator molding diameter as an average of these measurements.
- 6. Calculate the bulk density of the ablator molding in pounds per cubic foot $(1b/ft^3)$.

Ablator Molding Post-Cure Cycle

- 1. Post-curing of one to three ablator moldings can be performed simultaneously. When two or three ablator moldings are post-cured at the same time, surface thermocouple No. 3 (Program Controller), as described in paragraphs 2 and 3 below, shall be bonded to one of the ablator moldings only.
- 2. Instrument the ablator molding with three ball junction, No. 30 gage, chromel-alumel thermocouples, 15 feet long. Place one (1) thermocouple in the bottom of the cavity created by the thermocouple temperature probe. Pack the cavity with quartz felt. Bond the other two thermocouples side by side, approximately 1/2 inch to 3/4 inch apart 2 inches in from the outer edge. Bond thermocouples to the surface of the ablator with Saueresein No. 1. Air-dry the ceramic cement, and allow cement to cure at room temperature for 4 hours.
- 3. Number the thermocouple secured in probe cavity No. 1, and connect it to the Honeywell-Brown recorder. Number the two outside surface thermocouples No. 2 and No. 3. Connect No. 2 to the Honeywell-Brown recorder. Connect No. 3 to the program controller as the control thermocouple. Note that thermocouple No. 3 is required on only one ablator molding if more than one ablator is being post-cured at the same time.

- 4. Place the ablator molding(s) in an oven retort in an air-circulating oven. Hook up argon line from retort to argon source. Adjust the argon flow to the retort at eight retort volumes per hour, or 25 ±5 cubic feet per hour.
- 5. Set up the program controller, which is controlled by thermocouple No. 3, as follows:
 - (a) Raise temperature from 100° to 300° F at the rate of 5° F per hour.
 - (b) Hold at 300° F for 22 hours.
 - (c) At the end of 22 hours, turn off heating elements of oven but keep oven blower on. Allow oven to cool to 100° F.
- 6. To conform to the acceptance criteria of this procedure, the molded ablator shall meet the following post-cure specifications:
 - (a) The ablator molding shall be heated from 100° F to 300 \pm^0_{15} ° F at a uniform rate as indicated by thermocouples No. 1 and No. 2.
 - (b) The temperature of probe thermocouples No. 1 and No. 2 shall be at post-cure temperature for a minimum of 6 hours.
 - (c) The ablator molding shall be oven-cooled from 300 ± 0.0 F to 275 ± 0.0 F, as indicated by probe cavity thermocouple No. 1. Remove ablator molding from retort and place in an insulated container. Allow it to cool to room temperature.
- 7. Remove ablator from insulated box, remove thermocouple leads, and package ablator in a polyethylene bag. Reidentify with embossed aluminum tag on outside of bag.
- 8. Remove oven program chart and Honeywell-Brown recording chart from recording instruments. Draw a graphical plot of timetemperature curves of each thermocouple plot on a single graph. Identify the graph as form RE9, figure 38. Record on the graph and recording charts the date, job order, formulation batch number, and ablator molding number. Attach graph and charts to form RE6 of this procedure.

Post-Cure Density Determination

- 1. Perform and record density calculations in accordance with paragraphs 1 through 6 under Post Mold Density Determination.
- 2. Reseal ablator molding in polyethylene bag.

	TRANSDU	CER 1	TRANSDUCER 2		
	Up-	Down-	Up-	Down-	
Standard	scale	scale	scale	scale	
pressure	reading	reading	reading	reading	
. 200	200	210	200	200	
1,000	990	1,020	1,020	1,020	
2,000	2,015	2,060	2,040	2,040	
3,000	3,075	3,115	3,060	3,060	
4,000	$\frac{4}{5},075$	4,115	4,060	4,060	
5,000	5,080	5,120	5,055	5,060	
6,000	6,060	6,090	6,035	6,035	
7,000	7,060	7,080	7,020	7,030	
8,000	8,040	8,055	8,010	8,010	
9,000	9,030	9,040	8,990	8,995	
10,000	10,000	10,000	9,990	9,990	
	TRANSDU	CER 3	TRANSDI	UCER 4	
	Up-	Down-	Up-	Down_	
Standard	scale	scale	scale	scale	
pressure	reading	reading	reading	reading	
200	200	200	200	1 90	
1,000	1,035	1,030	950	960	
2,000	2,050	2,050	1,905	1,940	
3,000	3,080	3,070	2,910	2,960	
4,000	4,085	4,075	3,910	3,960	
5,000	5,065	5,060	4,940	4,990	
6,000	6,045	6,045	5,940	5,990	
7,000	7,030	7,045	6,960	7,000	
8,000	8,005	8,040	7,930	8,000	
9,000 10,000	$9,020 \\ 9,995$	9,050 9,995	8,990 9,990	$8,985 \\ 9,990$	
	TRANSDU		TRANSDI		
a. 1 1	Up-	Down_	Up-	Down_	
Standard	scale	scale	scale	scale	
pressure	reading	reading	reading	reading	
200	200	215	200	190	
1,000	1,080	1,065	1,050	1,045	
2,000	2,160	2,130	2,095	2,090	
3,000	3,190	3,165	3,135	3,130	
4,000	4,160	4,140	4,140	4,150	
5,000	5,145 6,140	5,120	5,140 6,130	5,145	
6,000	6,140	6,080	6,130	6,125	
7,000	7,085	7,055	7,110	7,110	
8,000	8,040	8,045	8,080	8,070	
9,000 10,000	9,010 9,960	9,000 9,960	$9,045 \\ 10,000$	9,045	
10,000	9,900	5,500	10,000	10,000	

ABLATION NOSE CAP							
Molding No.							
1	2	3	4	5	6		
LRC batch control number	batch	Ablator post mold weight (1b)	diameter		volume		
7	8	9	10	11	12		
Post mold density (lb/ft ³)	Post cure weight (1b)		diameter	Post cure volume (ft ³)	density		
Raw Materials Weight 25 percent phenolic resin, BRP-5549: grams,							
40 percent r	nylon powder, ohenolic micro	MP and DS Zytel 103: MP and DS oballoons, E	Material (grams, Material (Control No Control No grams,			
Raw mat. moi	isture conten	t Before	drying	After	drying		
Matei	rial type	Sample No.	% Moisture	e Sample No.	% Moisture		
Nylon powder	c						
Phenolic res	sin						
NOTE: Attac 1. I 2. (3. (4. I 5.	 Raw Material Sampling Forms for each of the three raw ingredients; reference form RE7. Graph of Ablator Cure Cycle; reference form RE8. Graph of Ablator Post Cure Cycle; reference form RE9. Pressure Transducer Recording Chart for Ablator Molding Cycle. Temperature Recording Chart for Ablator Molding Cycle. 						

Form RE6

SCOUT REENTRY HEATING PROJECT	Sample No.
MP and DS Sample Log Sheet	
Material Designation	
Manufacturer	
Date Received	
Batch Number	
Lot Number	
LRC Order No	
MP and DS Purchase Control No	
Date Sample Taken	
Storage Drum Zone No	
Relative Humidity During Sampling	
Temperature During Sampling	
MP and DS Batch Formulation No	
Sample Taken By	

Form RE7

Figure 25. Raw Materials Sampling Log

			IPC mo	isturo	content				
Ablator	Mat.	Nv	lon l	IStule		alloons	Hughes	Aircra	ft samples
molding	batch	Not	1011	Phen.	Not	LITOONS	nagnes	Phen.	Micro-
No.	No.	dried	Dried	resin	dried	Dried	Nylon	resin	balloons
NO.	NO.	ui icu	Direc	Testin	ur reu	Direu	NyTon	103111	barrooms
1	1	3	АЗ	1	2	A2	3	1	2
$-\frac{1}{2}$	2	4	A4	5	6	A6	4	5	6
2 3	3	7	A7	8	9	A9	7	8	9
4	4	10	A10	11	12	A12	10	11	12
5	5	13	A13	14	15	A15	13	14	15
6	6	16	A16	17	18	A18	16	17	18
7	7	19	A19	20	21	A21	19	20	21
8	8	22	A22	23	24	A24	22	23	24
9	9	$\frac{25}{25}$	A25	26	27	A27	25	26	27
10	10	28	A28	29	30	A30	28	29	30
11	11	31	A31	$\frac{32}{32}$	33	A33	31	32	33
12	12	34	A34	35	36	A36	34	35	36
13	13	37	A37	38	39	A39	37	38	39
14	14	40	A40	41	42	A42	40	41	42
15	$\overline{15}$	43	A43	44	45	A45	43	44	45
16	16	46	A46	47	48	A48	46	47	48
17	17	49	A49	50	51	A51	49	50	51
18	18	52	A52	53	54	A54	52	53	54
19	19	55	A55	56	57	A57	55	56	57
20	20	58	A58	59	60	A60	58	59	6 0
21	$\frac{20}{21}$	61	A61	62	63	A63	61	62	63
22	$\frac{21}{22}$	64	A64	65	66	A66	64	65	66
23	23	67	A67	68	69	A69	67	68	69
24	$\frac{23}{24}$	70	A70	71	72	A72	70	71	$\cdot 72$
25	$\frac{25}{25}$	73	A73	74	75	A75	73	74	7 5
26	$\frac{26}{26}$	76	A76	77	78	A78	76	77	78
27	$\frac{27}{27}$	79	A79	80	81	A81	79	80	81
28	28	82	A82	83	84	A84	82	83	84
29	29	85	A85	86	87	A87	85	86	87
30	30	88	A88	89	90	A90	88	89	90
31	31	91	A91	92	93	A93	91	92	93
32	32	94	A94	95	96	A96	94	95	96
33	33	97	A97	98	99	A99	97	98	99
34	34	100	A100	101	102	A102	100	101	102
35	35	103	A103	104	105	A105	103	104	105
36	36	106	A106	107	108	A108	106	107	108
37	37	109	A109	110	111	A111	109	110	111
38	38	112	A112	113	114	A114	112	11 3	114
39	39	115	A115	116	117	A117	115	116	117
40	40	118	A118	119	120	A120	118	119	120
41	41	$\frac{121}{121}$	A121	122	123	A123	121	122	123
42	$4\overline{2}$	124	A124	125	126	A126	124	125	126
43	43	$\frac{127}{127}$	A127	$\frac{1}{128}$	129	A129	127	128	129
44	44	130	A130	131	132	A132	130	131	132
45	45	133	A133	134	135	A135	133	134	135
				•	•		_	, –	
									· · · · · · · · · · · · · · · · · · ·

Figure 26. Ablator Molding and Materials Sampling Numbering Sequence

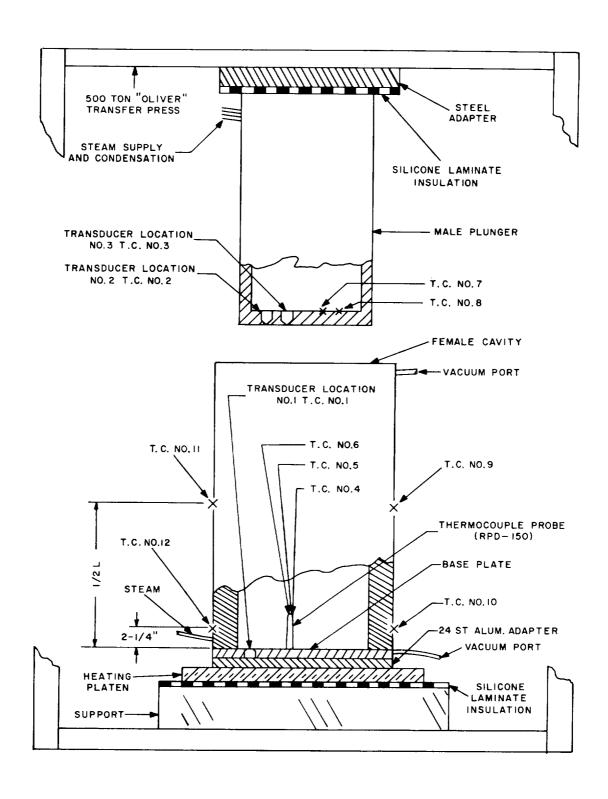
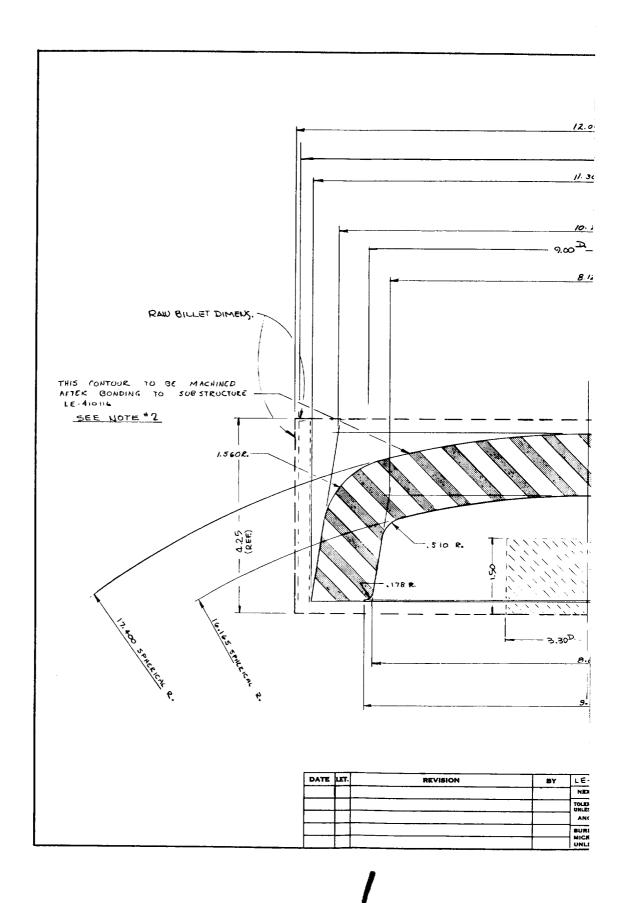


Figure 27. Sketch No. 1. Thermocouple and Pressure Transducer Location

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			NAMES OF
			-
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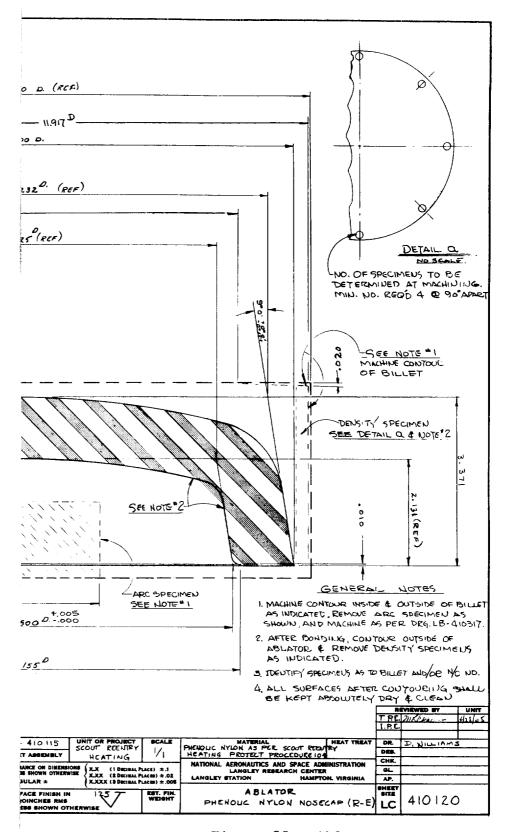


Figure 28. Ablator Contour.



1		

BONDING

PROCEDURE 105

Phenolic Nylon Nosecap

The procedural steps listed below must be followed to assure proper bonding of the ablator to the substructure.

- 1. Reference Drawings:
 - (a) Nosecap assembly dwg No. LX-410115
 - (b) Ablator retainer ring, dwg No. LB-410305
- 2. Materials Required:
 - (a) Ablator, LRC dwg No. LD-410120
 - (b) Tungsten substructure LRC dwg No. LE-410116
 - (c) Adhesive, tape supported, type HT-424, American Cyanimid Company, Bloomingdale Department, MP and DS Control No. B43-13C.727.L66617/C.
 - (d) Primer, type HT-424, 30-percent solids, Parts A and B, American Cyanimid Company, Bloomingdale Department, MP and DS Control No. B43-11C.727.L66617/C.
 - (e) Thinner, type HT-424, American Cyanimid Company, Blooming-dale Department, MP and DS Control No. B43-14L.727.L66617/C.
 - (f) Freon precision cleaning agent, E. I. DuPont.
 - (g) Methylethylketone solvent, Federal Stock No. 6810-281-2762.
 - (h) 1/4-inch-diameter silicone rubber stock.
 - (i) 1/16-inch-thick silicone rubber sheet stock, 1/8-inch-thick silicone sponge rubber sheet stock.
 - (j) 120-grit aluminum oxide abrasive grain.
 - (k) Iron-constantan thermocouple wire, No. 30 gage, certified calibration.
 - (1) Powdered asbestos.
 - (m) Pressure sensitive teflon tape, 3.5 mils.
 - (n) Silicone rubber, RTV-60, G.E. Co.
 - (o) DC274 adhesive, Dow-Corning
 - (p) Thermoflex felt, Johns-Manville Company.
 - (q) Teflon, 12 inches wide, 0.003 inch thick.
 - (r) Aluminum foil, soft, 8 mil thick.
 - (s) Masking tape, FSN 7510-266-6712
- 3. Fabrication Equipment Required:
 - (a) Blackstone ultrasonic degreaser, Model VR-20-3.
 - (b) Press, Stokes Model 727-1, 100-ton capacity, steam-heated platens.
 - (c) Honeywell-Brown recorder, 0 600° F, iron-constantan.
 - (d) Pangborn siphon blast cabinet.

- (e) Hand type blasting gun.
- (f) Shadowgraph scales, Model 4112-HB.
- (g) Oven, air-circulating, $0 600^{\circ}F$.

Bond Line Check Procedure

NOTE

The ablator, when not being processed, shall be placed in a clean polyethylene bag and stored in an environmental controlled area. The environment of the controlled area shall be as follows: Temperature, 7.2° F Relative Humidity, $60\% \pm 10$

- 1. Vapor-degrease tungsten substructure in Blackstone vapor degreaser, using freon precision cleaning agent, as follows:
 - (a) Vapor-rinse with distilled freon at $118 \pm 5^{\circ}$ F for 5 ± 1 minutes.
 - (b) Ultrasonic-clean with distilled freon at 105 \pm 50 F for 5 \pm 1 minutes.
 - (c) Vapor-rinse with distilled freon at $118 \pm 5^{\circ}$ F for 5 ± 1 minutes.
- 2. Cut from 8-mil soft aluminum foil four shims, 1/4-inch square. Position the shims 90-degrees apart on the tapered surface of the tungsten substructure, approximately 1/2-inch from the substructure flange. Tape the shims in place with 3.5-mil teflon tape.
- 3. Cover the inside contoured ablator surface with 3.5-mil teflon, 1-inch wide, pressure-sensitive tape. Overlap edges of the tape approximately 1/16 inch. Apply tape so that no air is entrapped between it and the ablator surface.
- 4. Cut from a 1/2-inch aluminum sheet a washer having an inside diameter of 7 inches and an outside diameter of 12 inches. This washer shall be used as the top pressure plate.
- 5. Cut from a 1/2-inch aluminum sheet a bottom pressure plate, 12 inches square.
- 6. Place a 1/16-inch-thick, 12-inch-square sheet of silicone rubber on the bottom pressure plate. Position the ablator on top of the silicone sheet.
- 7. Assemble the substructure in the ablator. Position the top pressure plate (refer to paragraph 4) on top of the substruc-

ture. Dead-weight the assembly with lead shot to ensure intimate contact between shims on substructure and ablator surface.

- 8. At four points, 90-degrees apart, measure the gap between the top pressure plate and the ablator. Cut from aluminum four suitable-thickness shims. Position these shims on the ablator surface. The shims shall be used as stops during the bond line casting operation. Remove the top pressure plate and substructure from the ablator.
- 9. Weigh out and mix 100 grams of RTV-60 silicone rubber catalyzed with 1 percent by weight of Thermolite T-12 catalyst.
- 10. Brush a generous uniform coat of RTV-60 silicone rubber on the bond area surface of the substructure.
- 11. Assemble the substructure in the ablator. Position the top pressure plate (refer to paragraph 4) on top of the substructure. Lightly clamp the assembly, using "C" clamps, until the top pressure plate lands on the four aluminum stops (refer to paragraph 8).
- 12. Cure the silicone rubber at 72° F and 58% relative humidity for 16 ± 2 hours.
- 13. Disassemble the substructure from the ablator, and remove the silicone rubber bond line from the substructure. Remove the shims from the substructure and the teflon tape from the ablator.
- 14. Divide and cut the silicone rubber bond line into eight equal pie-shape segments. Check the thickness of each segment along the cut edge with micrometers. Add 3.5 mils to the micrometer readings to compensate for the teflon tape used on the ablator during casting.
- 15. The bond line as checked by this method shall be 0.015 ± 0.003 of an inch.

Tungsten Substructure Surface Preparation

- 1. Vapor-degrease the substructure in the Blackstone vapor degreaser using freon precision cleaning agent as follows:
 - (a) Vapor-rinse with distilled freon at $118 \pm 5^{\circ}$ F for 5 ± 1 minutes.
 - (b) Ultrasonic-clean with distilled freon at $105 \pm 5^{\circ}$ F for 5 ± 1 minutes.
 - (c) Vapor-rinse with distilled freon at $118 \pm 5^{\circ}$ F for 5 ± 1 minutes.
 - (d) Remove substructure from degreaser and package in a clean polyethylene bag. White cotton gloves shall be worn for this operation and for all subsequent operations performed on the tungsten substructure.

- 2. Remove the substructure from the polyethylene bag, and mask off all areas outside of bond area with several layers of masking tape.
- 3. Using a hand-type blasting gun, uniformly blast the exposed bond area of the substructure with 120-grit aluminum oxide abrasive grain using 20-psig line air pressure. The line air to the blasting gun shall be filtered through a water separator to remove all moisture.
- 4. Remove masking tape. Remove all abrasive residue from surfaces of substructure with a filtered, moisture-free airstream.
- 5. Vapor-degrease as directed in paragraph 1 above.
- 6. Within 8 hours after abrasive cleaning operation, prime substructure bond area with HT-424 primer, as follows:
 - (a) Remove HT-424 primer from cold storage and allow it to come up to room temperature.
 - (b) Weigh out equal parts by weight of HT-424 primer, parts A and B, on shadowgraph scales and thoroughly mix, using a clean wooden spatula.
 - (c) Thin the mixed primer with 50-percent by weight of HT-424 primer thinner and thoroughly mix. The mixed primer shall be used within 4 hours after mixing. Store the mixed primer in a sealed container to prevent solvent evaporation.
 - (d) Apply a uniform brush coat of HT-424 primer to the prepared bond area of substructure, lightly brushing during application.
 - (e) Air-dry the primer for 35 ± 5 minutes at room temperature.
 - (f) Apply a second brush coat of primer as in step (d), above.
 - and air-dry as in step (e) above.
 Place the substructure in a preheated air-circulating oven, (g) and force-dry the primer for 60 ± 5 minutes at 150 $\pm 5^{\circ}$ F. Cool to 100° F $\pm 20^{\circ}$ F and remove from oven.
 - (h) Package the substructure in a polyethylene bag and store at room temperature.

Ablator Surface Preparation

- 1. White cotton gloves shall be worn for all operations while handling the ablator.
- Clean the contoured interface bond area of the ablator by spray-2. flushing the surface with distilled freon at 118 ±5° F. Dry the ablator in a preheated air-circulating oven at 125 ± 100 F for 60 ± 10 minutes.

- 3. Using a hand-type balsting gun, uniformly blast the ablator bond area surface with 120-grit aluminum oxide abrasive grain using 20 psig line air pressure. The line air shall be filtered through a water separator to remove all moisture.
- 4. Remove all abrasive residue from ablator surfaces with a filtered moisture-free airstream.
- 5. Prime the ablator surface bond area as given for the substructure.

Assembly of Components for Bonding

- 1. White cotton gloves shall be worn for all assembly operations.
- 2. Remove the HT-424 adhesive from cold storage and allow it to come up to room temperature.
- 3. Cut from the adhesive roll a 15-inch diameter disc. Remove the polyethylene backing from one surface. Remove the substructure from the storage bag, and center the exposed adhesive side onto the primed surface of the tungsten substructure. Remove the polyethylene backing from other surface of adhesive film.
- 4. Carefully fit the adhesive film to the contour of the tungsten substructure, smoothing out all wrinkles and excluding air entrapment between adhesive film and substructure. Trim off excess adhesive film at outside edge of substructure.
- Install an iron-constantan, No. 30-gage ball junction-type ther-5. mocouple, 15 feet long, in each of the four bored holes of the substructure numbered TC No. 19, 3, 5 and 25 (dwg No. LX-410115). To make the installation, slit the HT-424 adhesive film at the center of the hole. Insert the thermocouple lead through the hole from the back face and through the slit. Bend the ball junction to form a 90° angle to the thermocouple wire. Press the ball junction into the surface of the adhesive to hold it in position. Check to ensure that the thermocouple ball of each thermocouple does not extend outside the hole area. Tape the thermocouple to the inside contoured face of the substructure. Thread the free end of the thermocouple through any one of the drilled holes located on, and parallel to, the substructure flange.
- 6. Spot-weld three No. 30-gage iron-constantan thermocouples 15-feet long, to the tungsten substructure at thermocouple location No. 6, 7, and 8 (reference LRC dwg No. LX-410115). Locate thermocouple No. 6 on the inner surface at the center point of the substructure. Locate thermocouples No. 7 and 8 on the 9.125-inch-diameter surface of the substructure, 180° apart. Thread the free end of thermocouple No. 6 through any one of the

drilled holes located on, and parallel to, the substructure flange. Tape all leads to the substructure with heat-resistant tape. Position the ablator over the tungsten substructure in intimate contact with the adhesive film.

7. Pack powdered asbestos in the holes of the substructure where the thermocouples are located. Fill all other holes through substructure that are covered by the adhesive film with cured silicone rubber stock. Trim the silicone rubber stock approximately 1/4-inch above substructure surface for easy removal after bonding operation.

Assembly of Ablator Substructure in Molding Press

- 1. Position bottom steam platen only in Stokes 100-tone molding press, and hook up steam lines to platen.
- 2. Position and center the ablator substructure assembly on the heating platen, with the tungsten substructure resting on the bottom heating platen. Slip the ablator retainer ring (reference dwg No. LB-410305) over ablator and shim from bottom platen with wedges, so that it is centered on the ablator; a piece of neoprene rubber must be placed between the wedge and the ablator retainer ring.
- 3. Lightly tamp 3/8- to 1/2-inch-thick Thermoflex style RF-400 felt, around the periphery of the substructure, in any gap between the substructure and the platen.
- 4. Cut from 1/8-inch silicone sponge or 1/16-inch nonsponge rubber sheet stock a 12-inch diameter disc. Position the disc on top of exposed surface of ablator.
- 5. Connect the four bond line control thermocouple leads and the three substructure surface thermocouple leads to the Honeywell-Brown recorder in the following numbering sequence:
 - (a) Thermocouple location No. 19 to channel No. 1.
 - (b) Thermocouple location No. 3 to channel No. 2.
 - (c) Thermocouple location No. 5 to channel No. 3.
 - (d) Thermocouple location No. 25 to channel No. 4.
 - (e) Thermocouple location No. 6 to channel No. 5.
 - (f) Thermocouple location No. 7 to channel No. 6.
 - (g) Thermocouple location No. 8 to channel No. 7.
- 6. Switch on the Honeywell recorder and check each thermocouple for proper operation.

Adhesive Cure Cycle

- Record on the Honeywell-Brown recording chart the following information as it is developed:
 - (a) Date of cure.
 - (b) Time that heat cure cycle starts.
 - (c) Time that adhesive bond reaches $330 \pm 10^{\circ}$ F.
 - (d) Time that cure time at cure temperature starts.
 - (e) Time that cure time ends.
- 2. Calculate the load in pounds required to load the bond line area to 40 ±19 psi. For this calculation, use the reference 9.125-inch-diameter dimension to calculate the area to which the load will be applied. Close the molding press and apply 40 ±10 pounds per square inch (psi) to the assembly.
- 3. Raise the bond line temperature, as indicated by the lowest-reading control thermocouple, to $330 \pm 5^{\circ}$ F in 30 to 120 minutes.
- 4. Heat the bond line, as indicated by the lowest-reading control thermocouple, to $340 \pm 10^{\circ}$ F.
- 5. Cure the adhesive for 1 hour ± 10 minutes at 340 $\pm 10^{\circ}$ F.
- 6. Cool the bond line, as indicated by highest-reading control thermocouple, to $125 \pm {0 \atop 25}$ F under pressure with heat off.
- 7. Remove the bonded assembly from the molding press and disassemble the metal retainer ring. Remove the silicone rubber and thermocouples from the holes in the tungsten substructure.
- 8. Place the assembly in a clean polyethylene bag and forward to machine shop for contouring of the outer surface in accordance with dwg No. LC-410120.
- 9. Draw a graphical time-temperature plot of the cure cycle using form RE15. Attach it and the Honeywell-Brown recording chart of the cure cycle to this procedure.

Moisture Barrier

- 1. Place the contoured nosecap assembly, substructure side down, on a suitable pedestal to permit free access from all sides.
- 2. Mix equal portions, by volume, of DC-274 adhesive and toluene.
- 3. Using a stiff, short bristle brush, apply a uniform coating of the DC-274 adhesive on the nosecap ablator. Allow the adhesive to air-dry for 1 hour.

4. Cut a length of 0.003-inch teflon to cover the circumference of the ablator (approximately 42 inches); then brush a uniform coating of DC-274 adhesive on one side of the teflon, and allow to air-dry for 1 hour.

NOTE

When applying teflon to the ablator, it may be stretched slightly to prevent wrinkles; however, over-stretching will cause the teflon to creep after trimming.

- 5. Carefully place the teflon, adhesive side next to the ablator, around the circumference of the ablator, stretching slightly to prevent wrinkles. Overlap the teflon approximately 2 inches.
- 6. Using a soft cloth, carefully press the teflon around the side of the ablator and over the radius in such a manner as to prevent wrinkles or the entrapment of air.
- 7. Trim the teflon at the approximate center of the radius of the ablator.
- 8. Cut a piece of 0.003-inch teflon approximately 12 x 16 inches, coat one side with the adhesive, and allow it to air-dry for 1 hour.
- 9. Center the 12 x 16-inch piece of teflon, adhesive side face down, on top of the ablator. Starting at the center of the ablator and using a circular motion, firmly press the teflon to the ablator, progressing outward to the periphery. Stretch the teflon over the radius of the ablator and overlap approximately 3/4 inch. Trim excess teflon.
- 10. Place the teflon-covered ablator on a protected surface. Coat the bottom of the ablator with adhesive and allow to air-dry. Prepare a second piece of teflon as in step 8; when the adhesive has dried, cut an 8-3/4-inch disc from the exact center.
- 11. Stretch the teflon over the 9-1/8-inch diameter of the substructure and press it onto the ablator. With a soft, pliable, chisel-pointed tool, press the teflon into the corner of the substructure and ablator.
- 12. Fold the teflon over the ablator edge and overlap approximately 1/4 inch. Trim excess teflon and remove all excessive adhesive from the nosecap.
- 13. A capping strip of prepared teflon, 1/2 to 3/4-inch wide, may be placed over the two overlapping seams to assure a tight seal.

NOSECAP INSTRUMENTATION

PROCEDURE 106

Instrumentation Of Phenolic Nylon Nosecap

The procedural steps required to install the sensing devices in the nosecap are given below.

Reference Drawings:

- Nosecap assembly (dwg No. LX-410115) figure 33.
- (b) Spring wire ablation sensor, dwg No. LD-410119
- Optical light pipe ablation sensor, dwg No. LD-410118. (c)
- (d) Thermocouple sensor, dwg No. LD-410117.
- (e) Spacer (dwg No. LB-410123) figure 30.
- (f) Clamp, cable dwg No. LC-410121.
- (g) Retaining washer, (lwg No. LB-410124) figure 22.
- Wiring diagrams, (dwg No. LC-603899) figure 31 and (LC-(h) 604108) figure 32,
- (i) Substructure (dwg No. LE-410116) figure 34.

2. Materials Required:

- (a) Ablator (dwg No. LC-410120) bonded to substructure (dwg No. 410116) as shown on assembly dwg No. LX-410115.
- (b) Spring wire sensors.
- (c) Light pipe sensors.
- (d) Thermocouple sensors.
- (e) Cable clamps.
- (f) Retaining washers.
- (g) Spacers.
- (h) CIBA epoxy No. 6005 (Araldite),
- Versamid 140, reactive resin. (i)
- Plaster (quick-setting). Plaster form. (j)
- (k)
- (1) Vinyl tape.
- (m) Hygrograph paper.
- Thermistor, type GB-31J1. (n)
- (o) RTV-102 sealant.
- (p) Isofoam PE-2.
- (q) Shell Epon 931.
- (r) RTV-60.

3. Installation and Test Equipment Required:

- (a) Simpson test set, Model 262.
- (b) Milliammeter, 0.30 ma.
- (c) Depth gage, 0 to 3-in.
- (d) Feeler gage or shims.

- (e) Calipers or pin vise.
- (f) Resistance bridge (Rubicon).
- (g) Cavity inspection tool.
- (h) Micrometers, 0 to 3 inch.
- (i) GO-NO-GO gages, 0.245 through 0.255.
- (j) Hygrograph.
- (k) Precision spacing adapter, 1 inch.

Preinstallation Procedures and Measurements.

1. Measurements

- (a) Using a depth gage and the 1-inch precision spacing adapter, measure the depth ("A" dimension) of the thermocouple and light pipe holes on the nosecap. The depth shall be measured from the spot face area of the hole, to the hole bottom, along the center-line axis of the hole. Measure the hole diameter using GO-NO-GO gages. Record all measurements on the fabrication log, form RE4. Refer to dwg No. LX-410115.
- (b) Using a pin vise, measure the depth ("A" dimension) of the spring wire sensor holes. Record these measurements on form RE4, figure 29.
- (c) Using calipers, measure the total nosecap thickness ("C" dimension) at each hole. The measurement shall be made from the spot face area of the hole to the external surface of the ablator, along the center-line axis of the hole only. Record on form RE4.
- (d) Compute the remaining thickness, as the difference between the total thickness and hole depth, from the above measurements and record the result on form RE4 as the "X" dimension.

2. Plaster Mold for Nosecap

- (a) Prior to the preinstallation of the sensing devices in the nosecap, it is necessary to protect and support the external surface of the ablator.
- (b) Cover the ablator external surface with vinyl tape.
- (c) Prepare the quick-setting, low-shrink plaster in a form that will fit the nosecap.
- (d) Before the plaster sets, place the vinyl covered ablator into the plaster. Allow the plaster to set up firm.

3. Thermocouple Sensor Preparation

- (a) Measure the hole dimensions for hole numbers 3 through 29, and holes 46 and 47, record on form RE1. Compare with the measurements recorded on form RE4.
- (b) Select a thermocouple for hole location No. 3 by comparing the hole depth recorded on form RE1 and the plug length ("L") dimension recorded on form RE11. Measure the plug length and record on form RE1. Compute the washer shim thickness required by subtracting the hole depth from the plug length. Then subtract 0.002 inch from the computed difference and record on form RE11.
- (c) Using the hole diameter recorded on form RE4, compute and record on form RE11 the required plug diameter by subtracting 0.002 inch from the hole diameter.
- (d) Insert the thermocouple sensor, washer shim, protective cap, and form RE11 in a clean envelope and forward to machine shop for grinding.
- (e) Repeat steps (a) through (d) for thermocouple hole locations No. 4 through 29.

4. Light Pipe Ablation Sensor Preparation

- (a) Measure and record hole dimension for hole number 42 and record on form RE3-2. Compare with measurements recorded on form RE4.
- (b) Select the appropriate light pipe sensor for hole location No. 42; refer to dwg No. LD-410118. Verify the plug length and diameter by measurement, and record on form RE3. Compute the washer shim thickness by subtracting the hole depth from the plug length; then subtract 0.001 inch and record on form RE3. Grind the shim to this calculated dimension.
- (c) Perform the electrical measurement tests given in Procedure 102, steps 16 and 17. Record the results on form RE3.
- (d) Visually inspect the sensor for evidence of damage.
- (e) Repeat steps (a) through (c) for light pipe sensor holes No. 43 through 45.

Final Installation

1. Spring-Wire Sensor Installation

- (a) Select a spring-wire sensor of a length at least 0.010-inch greater than the depth of the hole in which it will be installed. Verify the sensor length and hole depth by measurement, and record on form RE2-2. Refer to dwg No. LX-410115.
- (b) With the Simpson test set, measure the resistance of the sensor. The resistance shall be $100 \text{K} \pm 10 \text{K}$. Record this measurement on form RE2-1. Observe polarity of leads.
- (c) Calculate, and record on form RE2-2, the required shim thickness from the difference between the sensor length and the hole depth. Select and use a shim of this size; refer to dwg No.LC-410123.

NOTE

The shim shall be nonmetallic to provide insulation between the sensor contacts and the substructure.

- (d) Carefully insert the sensor probe into the hole through the shim and into the ablator. When the sensor is properly bottomed, secure the sensor to the substructure with appropriate mounting hardware.
- (e) Record the sensor serial number and hole location number on form RE2-2.
- (f) Using the Simpson test set, again measure the resistance of the sensor and record on form RE2-1.

2. Thermocouple Sensor Installation

- (a) Select the thermocouple and the washer shim machined for hole location No. 19. Verify dimensions by measuring and recording on form RE11.
- (b) Using the Rubicon bridge, measure and record, on form RE-11, the thermocouple resistance. These readings shall be the same as previous measurements ±1 percent.
- (c) Apply a thin coat of epoxy bonding agent (CIBA 6005/Versamid 140) to the entire side of the thermocouple, from the shoulder to the face of the plug, being careful not to get any bonding on the thermocouple face.
- (d) Insert the thermocouple into the proper location hole, and press down until the thermocouple bottoms in the hole.

Secure the thermocouple in place with the washer shim and screws, making sure there is slight compression of the thermocouple in the hole when the shim is tightened on the backup structure.

- (e) For additional support, encapsulate the thermocouple leads with RTV-60 after installation.
- (f) Immediately measure and record, on form RE2, the resistances of the thermocouple. These readings shall be the same as previous measurements ± 1 percent.
- (g) Repeat the steps above for final installation of all subsequent thermocouples.
- 3. Installation of Thermocouple Sensors for Locations 46 and 47.

Thermocouple sensors T/C 46 and 47 were installed in the nose-cap after the installation of all other sensors (light-pipe, springwire, and thermocouple) was completed. The procedure used in the installation of thermocouple sensors T/C 46 and 47 is as follows:

- (a) The drilling areas for thermocouples T/C 46 and 47 were located in the nosecaps as shown on drawing No. LX-410115. Obstructing sensor leads were carefully moved and secured to provide safe access for the hole-drilling tool. The drilling areas were masked to prevent drilling chips and residue from entering the remaining instrumentated areas of the nosecap
- (b) The nosecap was secured to the boring-machine drilling jig. A vacuum-cleaning device was positioned adjacent to the drilling area to aid in removing drilling chips. Then the thermocouple location holes were drilled in accordance with drawing No. LX-410115. After drilling was completed, the nosecap was removed from the boring machine and cleaned.
- (c) The holes were then measured and their dimensions recorded on Form RE4. The nosecap was then placed in a protective storage container. Next, photographs were taken of the rear of the nosecap, and x-rays were taken of the new hole sites.
- (d) Thermocouple sensors were selected for installation by utilizing hole-depth dimension "A" as recorded on Form RE4, and plug-length dimension "M" as recorded on Form RE1. Dimension "M" is approximately 0.100-in. greater than the holed depth.
- (e) Utilizing the hole diameters recorded on Form RE4, the plug diameters were computed by subtracting 0.002-in. from the hole diameter, and recorded on Form RE1.

- (f) Using a Rubicon bridge, the thermocouple sensor resistances were measured and recorded on Form RE11.
- (g) A thin coating of epoxy bonding agent (60-percent CIBA 6005, 40-percent Versamid 140) was applied to the entire side of each thermocouple plug from the shoulder to the plug-base. The thermocouple plugs were then pressed into their respective holes until they bottomed. The thermocouples were temporarily secured in place by means of holding clamps.
- (h) The thermocouple resistances were again measured and recorded on Form RE2.
- (i) The exoxy bonding agent was permitted to air-dry at room temperature for 24 hours. The temporary holding clamps were then removed and RTV 102 was applied to the thermocouples to support and secure the cap ends.
- (j) The interconnecting sensor leads were then carefully dressed to and under the cable clamps (refer to dwg No. LX-410115). Photographs and x-rays were then taken of the completed T/C 46 and 47 locations.

4. Light-Pipe Sensor Installation

- (a) Select the light-pipe sensor and washer for hole location No. 42. Verify these dimensions by measurement and record on form RE3-2. Measure the resistance with the Simpson Model 262 on the 10K scale, observing polarity, and record the results on form RE3-1. The results should be the same as those previously recorded.
- (b) Apply a thin coating of Versamid 140/CIBA 6005 to the entire sensor plug length. Make certain that no bonding gets on the face surface of the sensor plug.
- (c) Carefully install the sensor into the proper location hole. Secure the plug in place with the retaining washer and mounting screws.
- (d) With the Simpson Model 262 test-set on the 10K scale, measure the resistance of the sensor. This measurement should be the same as that noted in step (a) above. Record this measurement and note any variation. Observe lead polarity.
- (e) Apply a small amount of RTV-60 to the back of the washer shim and wiring, to support the wiring where it passes through the shim.
- (f) Repeat the steps above for the final installation of all subsequent light pipe sensors.

(g) Fill void between spot face on backup structure and shoulder of light-pipe sensor with Epon 931.

5. Interconnecting Leads

- (a) Solder wire leads to the spring wire sensors. Connect the common terminals of each spring wire sensor together and solder to a common lead, in accordance with dwg No. LC-604108.
- (b) Dress all sensor leads under cable clamps and secure. Refer to dwg No. LX-410115.
- (c) Wire the common terminals of the light-pipe sensor together, in accordance with dwg No.LC-604108.
- (d) Color-code the light-pipe and spring-wire sensor leads as follows:

Systing Wire Sensors SW30 - Yellow SW31 - Blue SW32 - Green SW33 - Brown SW34 - Red, Yellow SW35 - Red, Blue SW36 - Red, Green SW37 - Red, Brown SW38 - Yellow, Blue SW39 - Yellow, Green SW40 - Yellow, Brown SW41 - Blue, Green

Light Pipe Sensors

LP42 - Black, Yellow, Blue LP43 - Black, Red, Yellow LP44 - Black, Blue, Green LP45 - Black, Green, Brown

LP Common - Black

SW Common - Red

6. Thermistor Installation

(a) Install one thermistor at hole location No. 1, and another at hole location No. 2 (reference dwg No. LX-410115), using RTV-102 sealant.

7. Repair and Replacement

(a) All repairs and/or replacement of any sensing device must be recorded on the back of form RE4. Use the appropriate procedure required for installation when replacement is necessary.

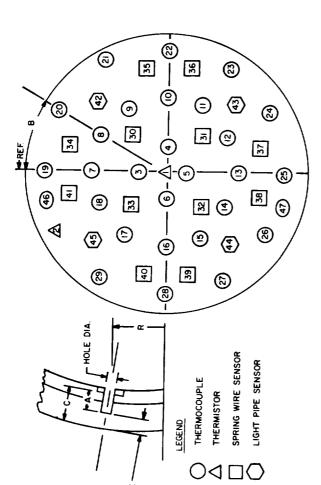
8. Connector Installation

(a) When all sensors are installed in the nosecap, dress the interconnecting leads under the cable retaining clamps; refer to dwg No. LX-410115.

(b) Terminate sensor cables with connectors, refer to dwgs No. LC-604108 and LC-603899.

9. Encapsulation

- (a) Prepare the nosecap for encapsulation by covering the retaining plate with teflon tape.
- (b) Assemble the retaining plate to the substructure with six screws.
- (c) Mix 50 grams of PE-2 foam (equal parts A and B) for approximately 30 seconds and pour through the vent holes in the retainer plate. Repeat several times until the cavity is filled. Allow the foam to harden approximately 5 minutes between pourings.
- (d) Permit the nosecap to set for one hour at room temperature before removing excess foam and the retainer plate.



"X" dimensions logged do not include 0.003" the Teflon moisture barrier The

Figure 29.

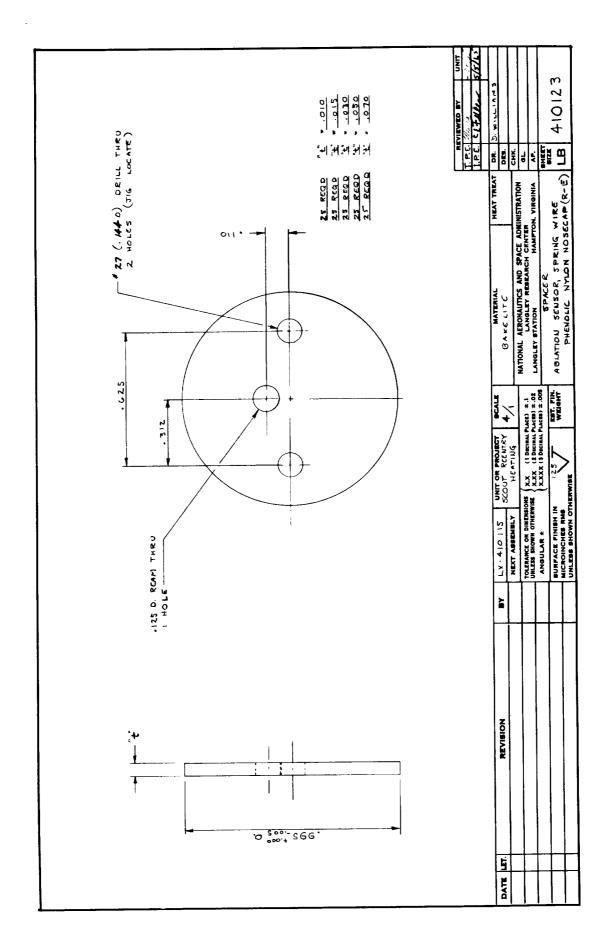
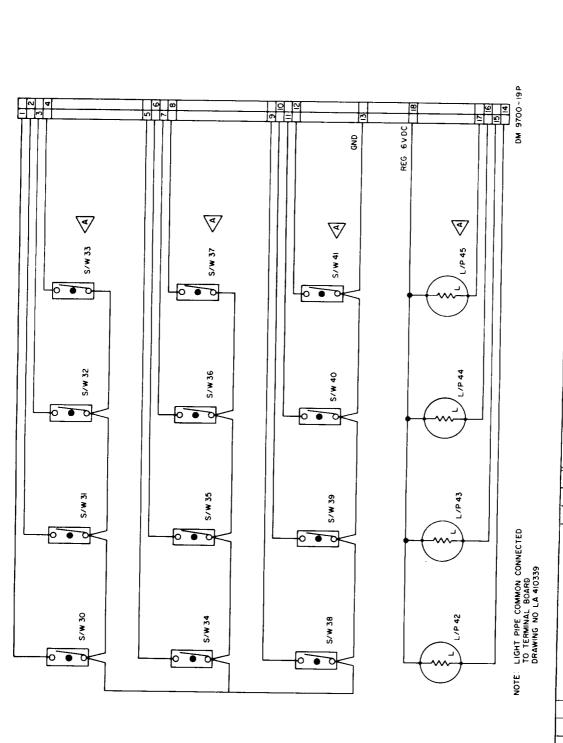
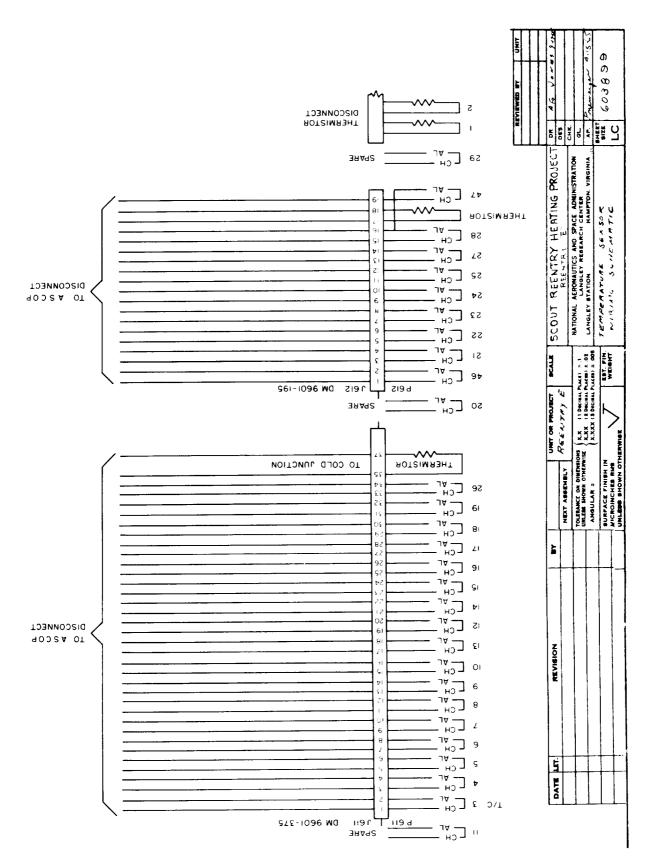


Figure 30. Spring-Wire Ablation Sensor Spacer

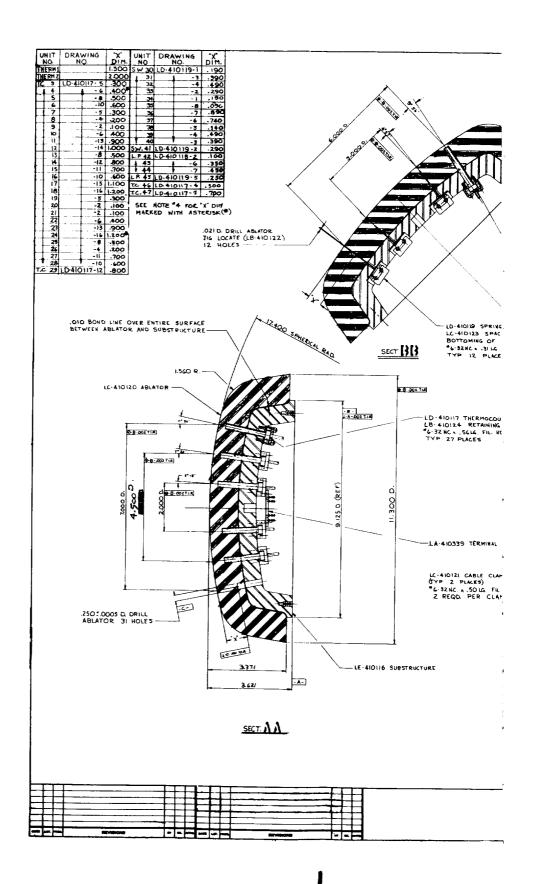


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Figure 31. Ablation Sensor Nosecap Wiring Diagram



gure 32. Temperature Sensor Wiring Schematic



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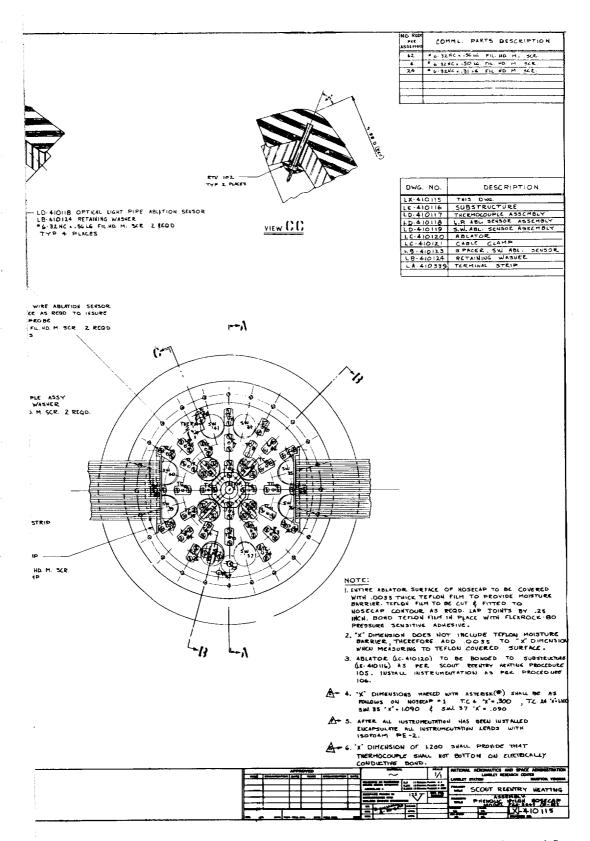
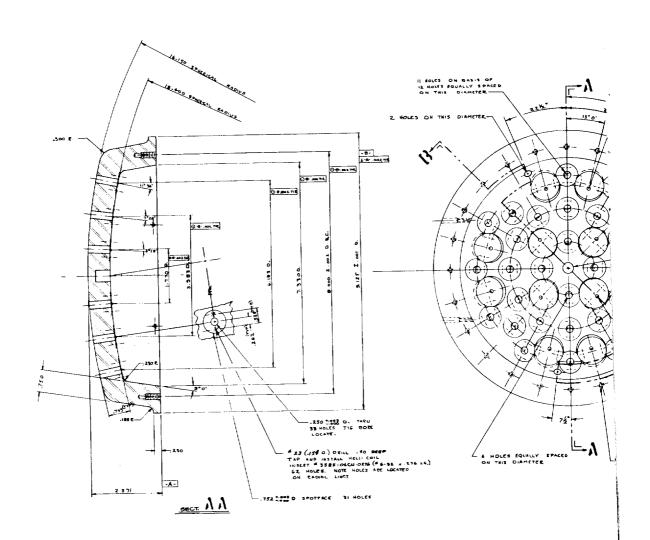
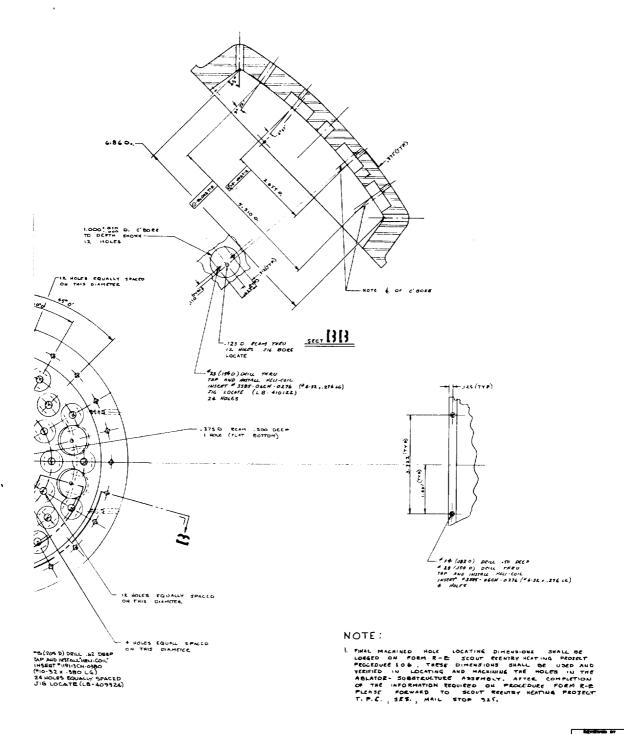


Figure 33. Phenolic Nylon Nosecap Assembly.



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Figure 34. Phenolic Nylon Nosecap Substructure.

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ARC JET TEST

PROCEDURE 107

Specimen Assembly

The procedure for performing arc-jet tests on 3-in. ablator material specimens is given below.

- 1. Reference Drawings:
 - (a) Arc-jet specimen, thermocouple (dwg No. LC-410128), figure 36.
 - (b) Arc-jet specimen, plug density variation (dwg No. LD-410271).
 - (c) Arc-jet specimen, constant plug density (dwg No. LD-410272).
- 2. Test Equipment Required:
 - (a) LRC 2500-kw arc-jet facility.
 - (b) 12-channel Minneapolis-Honeywell Visicorder.
 - (c) 18-channel C.E.C. recorder.
 - (d) LRC central digital data recording facility.

Sub-sonic Test Procedure

- 1. Install 4-in. nozzle on LRC 2500-kw arc-jet facility.
- 2. Mount the specimen on a water-cooled sting with the face of the specimen 2 inches from exit of arc-jet nozzle.
- 3. Mount a 3-in. diameter flat-faced heat flux calorimeter on a sting with the face of the calorimeter 2 inches from exit of arc-jet nozzle.
- 4. Connect the lead wires from the R-E Scout Project specimen and the calorimeter to the arc-jet junction board.
- 5. Prepare the instrumentation patch-board in accordance with Entry Structures Branch (ESB) procedures.
- 6. Check the electrical continuity of the sensor circuits.
- 7. Turn on the 18-channel C.E.C. recorder for the necessary warm-up period.
- 8. Calibrate the channels being used for recording heat flux on the 12-channel Minneapolis-Honeywell Visicorder.

9. In accordance with ESB procedures, establish the following test conditions:

Heating rate - 100 + Btu/ft²-sec Stream enthalpy - 2800 Btu/lb Mass flow rate - 0.35 lb/sec Oxygen concentration - 3 percent Stream velocity - subsonic Voltage tap - 2400 Power - 1800 kw 3 reactors - tap 2

Record the test conditions on test data form RE10, figure 35

- 10. Start the arc-jet facility in accordance with ESB procedures. Request confirmation of proper operation of facility at the required test conditions by ESB Test Coordinator.
- 11. Insert a calorimeter into the arc-jet stream for heat flux measurement. Allow photographic film from Visicorder to develop with jet operating, and determine the heat flux. If the measured heat flux is not in accordance with the value shown in step 9 above, terminate the test and request ESB Test Coordinator to conduct inspection of the arc-jet facility, calorimeter, and instrumentation.
- 12. If the measured heat flux conforms to the heat-flux requirement in step 9, insert the test specimen into the arc-jet stream. Terminate the test on command from the Project Engineer.
- 13. Determine the post-test heat flux in accordance with step 11.
- 14. Secure the arc-jet facility in accordance with ESB procedures. Remove the test specimen from the water-cooled sting and deliver it to the Project Engineer.

The procedure for performing arc-jet tests on 1-1/2-inch ablator material specimens is given below.

1. Reference Drawings:

Arc-jet specimen - materials performance (dwg No. LB-410317) figure 37.

- 2. Test Equipment Required:
 - (a) LRC 2500 kw arc-tunnel facility
 - (b) LRC central digital data recording facility

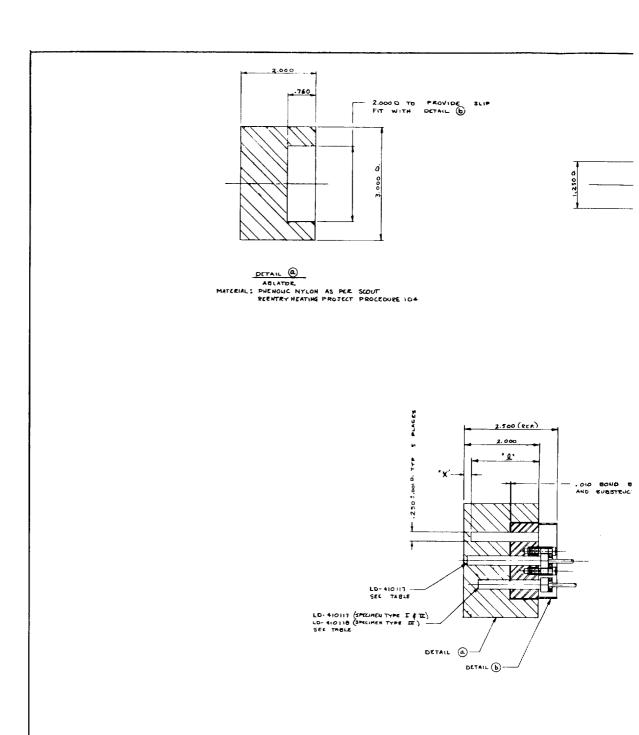
Super-sonic Test Procedures

- 1. Install supersonic nozzle with 1.500-in. minimum diameter in the 2.0-in. exit on the 2500-kw tunnel facility.
- 2. Mount the test specimen on a water-cooled sting with the specimen face spaced 0.5-in. from the tunnel nozzle exit.
- 3. Prepare the instrumentation patch board in accordance with ESB procedures for measuring arc tunnel conditions.
- 4. Check electrical continuity of sensor circuits.
- 5. Set the desired test conditions in accordance with ESB calibration procedures. Record the test conditions on test data form RE10 (figure 34).
- 6. Start the arc-tunnel facility in accordance with ESB procedures. Request confirmation of proper operation of facility at the required test conditions by the ESB Test Coordinator.
- 7. If visual indication of arc-chamber pressure mass flow rate and tunnel power is in accordance with ESB calibrations, insert the test specimen in the arc tunnel stream. Terminate the test on command from the Project Engineer.
- 8. Secure the arc-tunnel facility in accordance with ESB procedures. Remove the test specimen from the water-cooled sting and deliver it to the Project Engineer.

Tes	t Date: Test Data for Arc Jet Test Sheet No
1.	Project or test purpose
2.	Arc jet to be used Nozzle sizein. (Use separate sheet for eachin
	Specimen height above the nozzlein. nozzle)
3.	Approx. No. of runs with specimen Duration of each run
4.	Approx. No. of calibration runs sec.
5.	Special equipment to be used:
	(a) Oscillograph Yes No
	No. of channels Arrangement of channels
	Calibration M.V. Deflection inches
	Beckman, number of channels
	(b) Sting: Length diam. 7/8 inch diam. 3 inch
	(c) Calorimeter: 3/8 inch 3 inch flat 3 inch hemisphere
	(d) Camera: (1) FastaxB and WColor
	(2) 16 mm movie Frames per sec
	(3) Field of view
	(e) Other equipment required:
6.	flow rate required 1b/sec
7.	flow rate requiredlb/sec
8.	Heating rate requiredBtu/ft ² -sec
9.	Power requiredkw No. reactorsTop
 Rem	narks Tests completed Date

FORM RE10

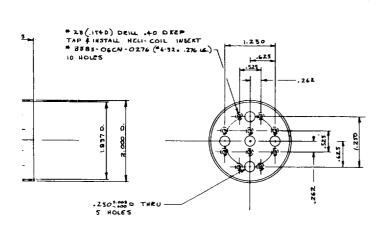
Figure 35. Arc Jet Test Data



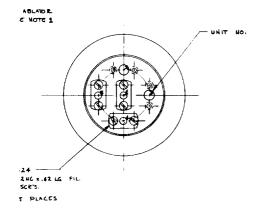
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DETAIL (b) SUBSTRUCTURE MATERIAL : TYPE 8+7 STAINLESS STEEL



UNIT	SPECI I			דואט	SPECIMEN TYPE IL			
NO.	DRAWING NO.	* X*	L. NOTE	NO.	DRAWING NO.	"X"	VOLC NOLC	
T.L. 1	LD-410117 - 2	.100	1.900	T.C. 1	LD-410117 - 17	.250	1.750	
1 2	1 -4	.200	1.800	4 2	A -17	į.	+	
3	-5	.3.00	1.700	3	-17			
1 4	٠- ١	.400	1.600	1 4	¥ -17	1	-	
T.C. 5	LD-+10117 - B	.500	1.500	T.C. 5	LD-410117 - 17	.250	1.730	
UNIT	SPECIME TYPE			SPECIMEN UNIT TYPE TO				
NO.	DRAWING NO.	*x*	HOLE YOLE	NO.	DRAWING NO.	,×,	L HOLE DEPTH	
T,C . 1	LD -410 117 - 17	. 250	1.750	1	DO NOT DRILL TH	IS HOLE IN	MALATO	
L.P 2	LO-+10118 - 1	.050	1.950	LP.Z	LD-410118-4	.200	1.800	
1 3	4 -2	.100	1.900	13	-2	.100	1.900	
+ 4	-3	.150	1.850	14	- 4	.200	1.800	
			1.800	1.85	LD-410118 -3	.150	1.850	

NOTE:

- 1. BOND SUBSTRUCTURE TO ABLATOR AS PER SCOUT RECUTRY HEATING PROTECT PROCEDURE 105 (HT 424)

 2. MEASURE AND RECORD "X" AND "L" DIMENSIONS ON FORM PROVIDED IN SCOUT RECHIRY HEATING PROTECT PROCEDURE 106

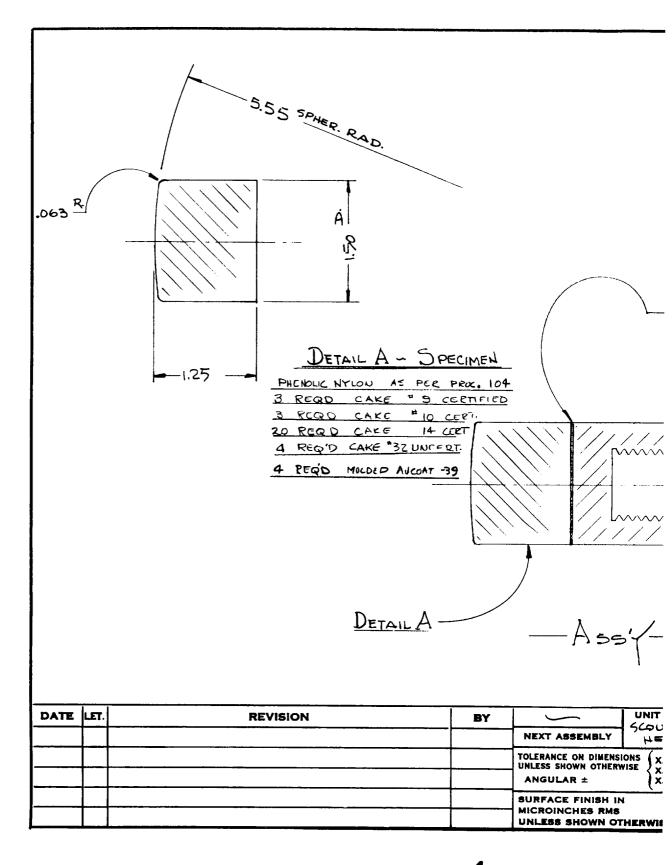
TOTAL 3 TYPE I SPECIMENS REQU TOTAL 3 TYPE II SPECIMENS REQD. TOTAL 2 TYPE III SPECIMEN REGD. TOTAL I TYPE TO SPECIMEN REOD.

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Figure 36. Phenolic Nylon Nosecap Arc-Jet Specimen.



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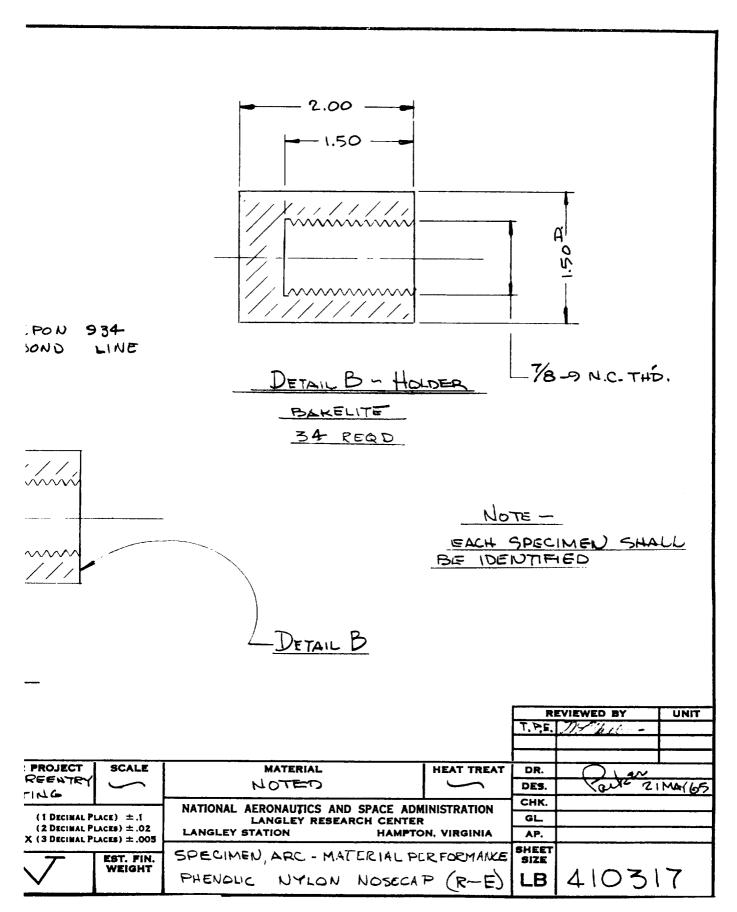


Figure 37. Phenolic Nylon Nosecap Arc Specimen,
Material Performance.



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FINAL DATA

All mechanical measurements and electrical data for nosecaps No. 1 and No. 2 were recorded on log sheets. These completed logs are made part of this report.

Appendix 1 of this report lists all assembly drawings required for the Reentry E project, and Appendix 2 contains calibration data for correlation with flight telemetry data.

Ablator

To verify that the ablator material used for the Scout Reentry Heating Project, Reentry E, had satisfied the requirements of this experiment, the molding process of the billet was carefully monitored. Specimens taken from the billet were subjected to the same arc-jet tests which established material requirements. The in-process checks consisted of monitoring and recording the temperature and pressure of the cure cycle. These checks were plotted on form RES, figure 38; the post-cure cycle of the ablator was also plotted and is shown in figure 39, for nosecap No. 2.

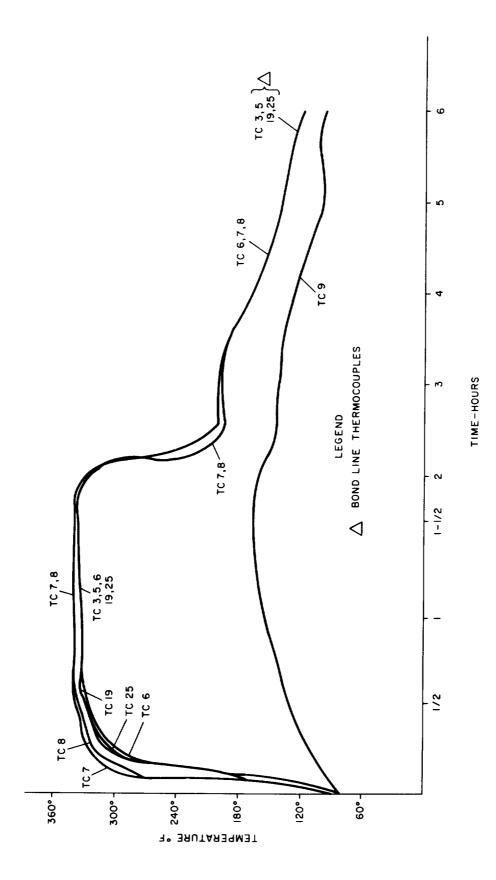


Figure 38. Cure-Cycle Graph, Nosecap No. 2

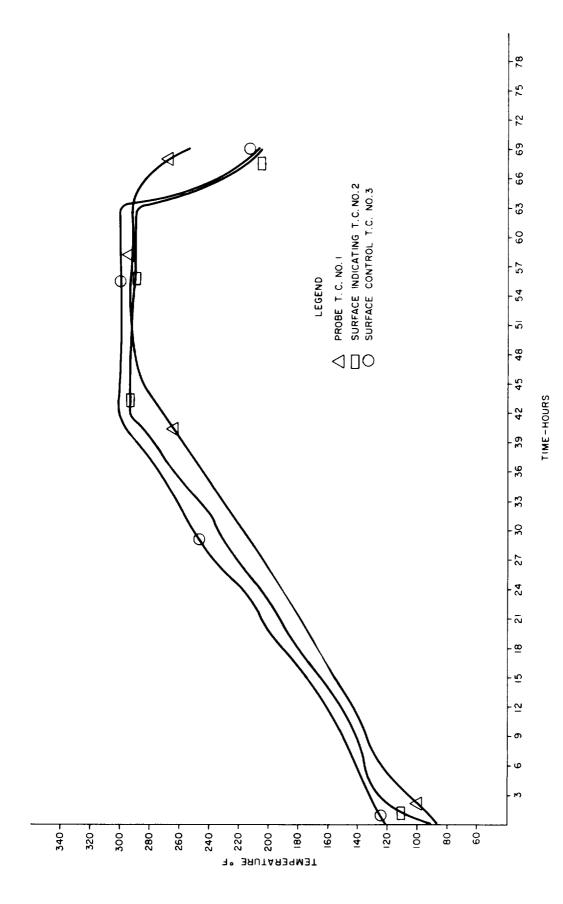


Figure 39. Post-Cure Cycle Graph, Nosecap No. 2

Bonding

The in-process monitoring of the bonding technique, to assure that a complete and stable bond line had been achieved, was accomplished by monitoring the temperature of the cure cycle. The bond line thickness was controlled as described in Procedure 105. After bonding, the nosecaps were X-rayed to assure a uniform bond. The bond line cure cycle was plotted on form RE5 and is shown in figure 40, for nosecap No. 2.

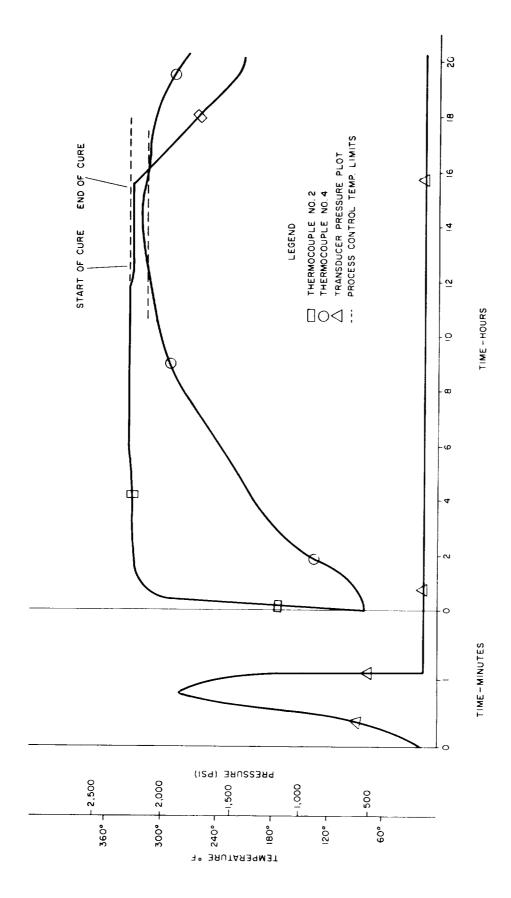


Figure 40. Bonding Graph, Nosecap No. 2

Nosecap Subassembly

Machining and drilling of the nosecap subassembly was accomplished in accordance with detailed assembly dwg No. LX-410115. All physical dimensions conformed to the drawing. The sensor mounting holes were measured and verified and were recorded on the fabrication log, form RE4, figure 41.

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HOLE DIA.	۳ ا	'		0.24	- 4	엑	0.24		2,70	-		0.749		4 4	- 4	- 1			0.249	-1	7,7	0.249		0.24	-	-4		0.24	4.	-1	0.02	1	0.02	3 0	ч.	0.02	-	4 -	- 4	4	0.021	0.24	0.249	
×	1.524	1.985		0.302	- 4	~1	0.602	.i	000	-	4	4 .	4 .	14		0.602	-1	1.206	0.301	-	300			0.502			0.601	-1	4 ⋅		0,197	<u>ان</u>	•	0.192			0.743		7	7	0.292	0.100	0.349	
æ	0	3.0795		0.885	- 4		.885	1.9915	200		1 9915		12		1.9915	1.9915	. 991	-1	0.0	•	4	3.0795		3.0795	3.0795	.079	3.0795	430	3		1.3275	1.3275	1.32/5	2.655	1 1	٠	S	.65	١ ١	3	2,655		2.655	1
O	1,990	1.985		1,990	- 1	1.989	-1	1.994	1	1	1 993	1.993	1.994	1.994	1,993	-1	•	1.992	1.985	1 200	1 986	1.986	1.986	1.986	1.988	1.987	1.987	7 143	-		1.617	•	/191/		1.620	1.620	1.62!	1,621	1.621		1.618	1.989	1.989	1
ø	0	330		0	90	180	270	2	2 6	9	120	150	180	210	240	270	300	330			9	120	150	180	210	240	0/7	337.5	1.		45	135	277	15	7.5	105	165	195	255	285	345	45	135	
V	995,	0		1,688	1.588	1.488	-1	707	1 805	1.022	1.091	0.990	· •	1,193	- 1	1.393	•1	!	1,084	1.009	1.587	1.084	0.781	1,484	1.789	1.286	1.586	42	6	1 1	1.220	1.225	1.120	1.427	1.532		0.878	1,481	1,127	1.232	1.326 1	1,889	1.640	1
SERIAL No.		-		NC5-9	NC6-6	NC8-8	NCIO-9	NC 2-11	NC2-10	NC6-8	NC13-9	1 .	NC8-10	NC12-5	NC11-6	NC10-11	NC 15-6	NC16-3	NC3-10	17	d r	NC13-7	NC16-2	NC8-9		<u>`</u>	NC10-10		C	1 1	122	126	127	123	135	132	131	130	CV	√4 :	135	LP 94	LP 93	ı
IH No.	-	2	I/C	~	4	Ŋ	٠	\ a		\ -	=	12	13	14	12	2	: ا	2 2	, j	3/5	22	23	24	2.5	56	27	202	94	47	S.W.	30	31	37 6	34	35	36	3.7	30	33	04.	1 7	42	43	

46 (9) (2) (4) (4) (3) (4) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	(4) (8) (9) (1) (1) (1) (1) (1) (1) (1) (1) (1) (1	(a) (a) (b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c	<u>—</u> @-	(36) 184 (37) (39) (47) (35) (49)
Lot of	X Y HOLE DIA. (3)	ī	(b)	LIGHT PIPE SENSOR

The "X" dimensions logged do not include 0,003" for the Teflon moisture barrier

Sensing Devices Installation and Measurement Log, Nosecap No. 2 Figure 41.

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Spring-Wire Ablation Sensor

During the fabrication of the spring wire sensors, all pertinent mechanical and electrical measurements were recorded on the sensor log sheet, form RE2-2, figure 42. At the time of installation in the nosecap, the hole location number and related data were recorded on the fabrication log, form RE4.

Installed Date: 9/1/65

SPRING-WIRE SENSOR INSTALLATION

NOSECAP NO. 2

Sensor		Length		F					
To End of Tube	pu	To End of Knot	Hole Number	Total Thick- ness of Nosecap	Hole Depth	kemain- ing Thick- ness "X"	Shim Thick- ness	Distance Surface to End of Tube	Hole Number
1,494	194	1.500	30	1.617	1.220	0.197	080.0	0.203	30
1.494	194	1.500	34	1,619	1.427	0.192	0.074	0.199	34
1.3	1.392	1,395	33	1.617	1.330	0.287	0.066	0.291	33
1.396	968	1.400	41	1.618	1.326	0.292	0.075	0.297	41
1.2	1.291	1.300	31	1.617	1.225	0.392	0.076	0.402	31
1.5	1.294	1.303	40	1.620	1.232	0.388	0.072	0.398	40
<u> </u>	1.195	1.203	32	1.617	1.120	0.497	0.083	0.505	32
1,194	194	1.203	39	1.621	1.127	0.494	0.077	0.504	39
.	1.540	1.547	38	1.621	1.481	0.140	0.067	0.148	38
0.5	0.944	0.947	37	1.621	0.878	0.743	0.070	0.747	37
0	0.796	0.802	36	1.620	0.732	0.888	0.071	0.895	36
1.	1.594	1.600	35	1.620	1.532	0.088	0.069	0.095	35
									٠

FORM RE2-2

Figure 42. Spring-Wire Sensor Installation

Light-Pipe Ablation Sensor

The results of electrical tests and mechanical measurements of the light-pipe ablation sensors after fabrication were recorded on form RE3-2, figure 43. Hole locations in the nosecap and related measurements during installation were recorded on form RE4.

LIGHT PIPE LOCATION

ASSEMBLY NO. NC No. 2

TANCE	Post Instal- lation	27.5K	30.5K	31.75K	29.5K			
SENSOR RESISTANCE	Pre-Instal- lation	27.5K	30.5K	31.5K	29.5K			
WASHER	Shim Thickness	0.265	0.264	0.262	0.262			
13)	"X"	0.100	0.349	0.452	0.247			
ASSEMBLY (MAT'L NO. 13)	Depth Meas.	1.889	1.640	1.538	1.741			
	Diam. Meas.	0.249	0.249	0.249	0.249			
ASSEMBI	Hole Number	42	43	44	45			
	Diam. Meas.	0.247	0.248	0.248	0.247			
Ē	"M" Length Measured	1.965	1.715	1.611	1.814			
LIGHT PIPE	"L" Length "M" Length Di	2.155	1,905	1.801	2.004			
	Mat'l No.	14C	14C	14C	14C			
	Serial Number	94	93	26	100			

FORM RE3-2

Figure 43. Light Pipe Location

Thermocouple Sensors

Pertinent measurements of individual thermocouple sensors were recorded on form RE1, figure 44. Tests results and mechanical dimensions were recorded on form RE1. Hole location numbers at installation were recorded on form RE4.

THERMOCOUPLE LOCATION

ASSEMBLY NO. NC NO.2

	THERN	THERMOCOUPLE (MAT'L No.	T'L No.)		ASSEMBLY		(MAT'L No.	. 13)	WASHER	FINAL	ELECTRICAL	AL RESISTANCE	STANC	BO
	Serial Number	"L" Length Measured	"M" Length Measured	Diam. Meas.	Hole Number	Diam. Meas.	Depth Meas.	"X"	Shim Thick- ness	Forward	Reverse	Chromel Leakage	Alumel Leakage	nel kage
15C	NC 5-9	1.942	1.752	0.247	က	0.249	1.688	0.302	0.252	19.38	19.38	8-	8-	
30	NC 6-6	1.848	1.658	0.247	4	0.249	1.588	0.401	0.258	18.43	18.43			
4C	NC 8-8	1.742	1.552	0.246	5	0.248	1.488	0.501	0.252	19.55	19.55			
15C	NC10-9	1.646	1.456	0.247	9	0.249	1.388	0.602	0.256	17.84	17.84			
4C	NC5-11	1.945	1.755	0.247	7	0.249	1,695	0.299	0.248	18.75	18.75			
15C	NC4-8	2.037	1.847	0.247	∞	0.249	1.794	0.200	0.241	19.66	19.66			
4C	NC2-10	2.144	1.954	0.247	6	0.249	1.895	0.099	0.247	18.64	18.64			
4c	NC6-8	1.845	1.655	0.247	10	0.249	1.593	0.400	0.250	19.03	19.03			
4c	NC13-9	1.340	1.150	0.247	11	0.249	1.091	0.902	0.247	Spe	Spare			
	NC14-3	1.240	1.050	0.247	12	0.249	0.990	1.003	0.248	18.42	18.42			
ı	NC8-10	1.745	1.555	0.247	13	0.249	1,493	0.501	0.250	19.87	19.87			
	NC12-5	1.444	1.254	0.247	14	0.249	1.193	0.801	0.249	20.56	20.56			
	NC11-6	1.537	1.347	0.247	15	0.249	1.291	0.702	0.244	20.81	20.81			
15C	NC10-11	1.638	1.448	0.247	16	0.249	1.393	0.602	0.243	20.52	20.52	 	->	
į.								-						1

Thermocouple Location (Sheet 1 of 2) Figure 44.

FORM RE1

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DATE Sept. 15, 1965

THERMOCOUPLE LOCATION

0 NC NO. ASSEMBLY NO.

	THERM	THERMOCOUPLE (MA	(MAT'L No.)		ASSEMBLY	1	(MAT-L No.	13)	WASHER	FINAL	ELECTRICAL	l	RESISTANCE
	Serial Number	"L" Length Measured	"M" Length Measured	Diam. Meas.	Hole Number	Diam. Meas.	Depth Meas.	"X"	Shim Thick- ness	Forward	Reverse	Chromel Leakage	Alumel Leakage
15C	NC15-6	1.139	0.949	0.247	17	0.249	0.890	1.102	0.247	21.13	21.13	8-	8
30	NC16-3	0.995	0.805	0.247	18	0.249	0.786	1.206	0.207	19.75	19.75		
15C	NC5-10	1.937	1.747	0.247	19	0.249	1.684	0.301	0.251	19.99	19.99		
4C	NC2-12	2.140	1.950	0.247	20	0.249	1.889	0.097	0.249	spare	re		
4C	NC2-13	2.142	1.952	0.247	21	0.249	1.887	0.100	0.253	19.73	19.73		
30	NC6-7	1.845	1.655	0.247	22	0.249	1.587	0.399	0.256	21.00	21.00		
4C	NC13-7	1.345	1.155	0.247	23	0.249	1.084	0.902	0.259	17.84	17.84		
30	NC16-2	0.987	0.797	0.249	24	0.251	0.781	1.205	0.204	18.66	18.66		
4C	NC8-9	1.743	1,553	0.247	25	0.249	1.484	0.502	0.257	19.30	19.30		
15C	NC4-7	2.044	1.854	0.247	56	0.249	1.789	0.199	0.253	20.73	20.73		
30	NC11-5	1,536	1.346	0.247	27	0.249	1.286	0.701	0.248	17.19	17.19		
15C	NC10-10	1.640	1.450	0.247	28	0.249	1.386	0.601	0.252	15.51	15.51		
3С	NC12-4	1.445	1.255	0.247	67	0.249	1.184	0.801	0.259	spare	ıre		
4C	NC4-10	2.045	1.855	0.247	46	0.249	1.642	0.501	N/A	17.60	17.60		
30	NC7-2	1.788	1.598	0.247	47	0.249	1.443	0.700	N/A	18.52	18.52	-	->

FORM RE1

BACKUP NOSECAP NO. 1 FINAL DATA

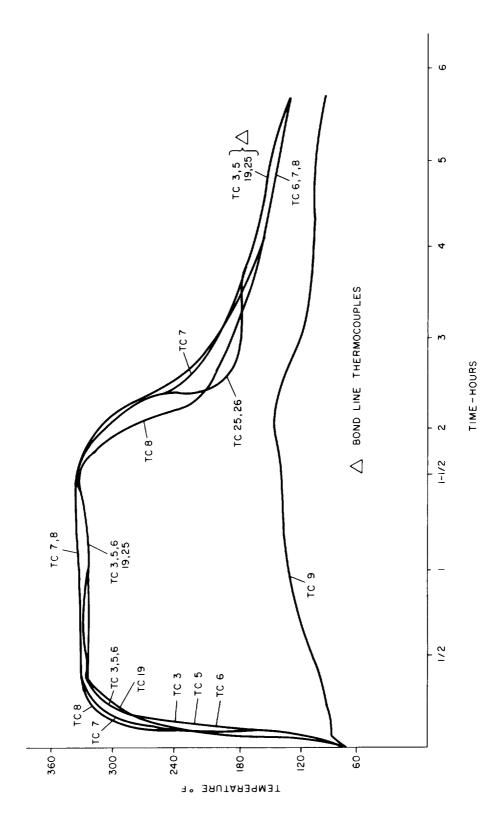


Figure 45. Cure-Cycle Graph, Nosecap No. 1

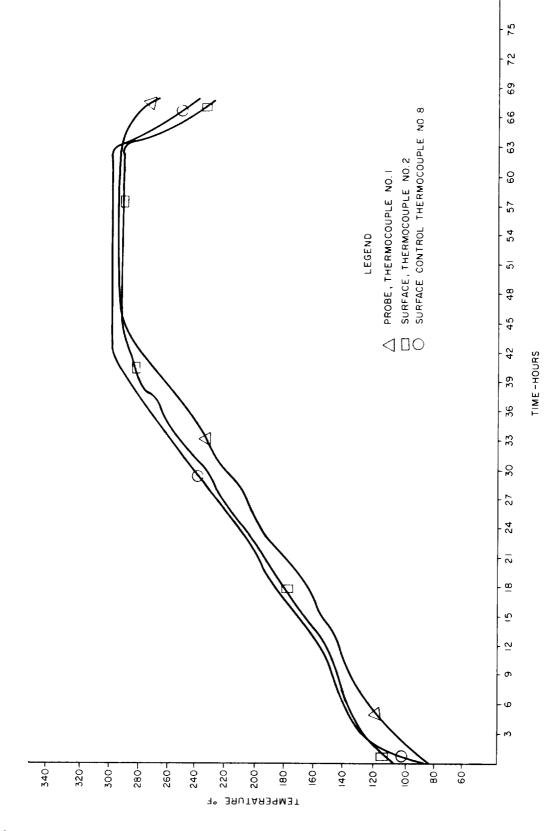


Figure 46. Post-Cure Cycle Graph, Nosecap No. 1

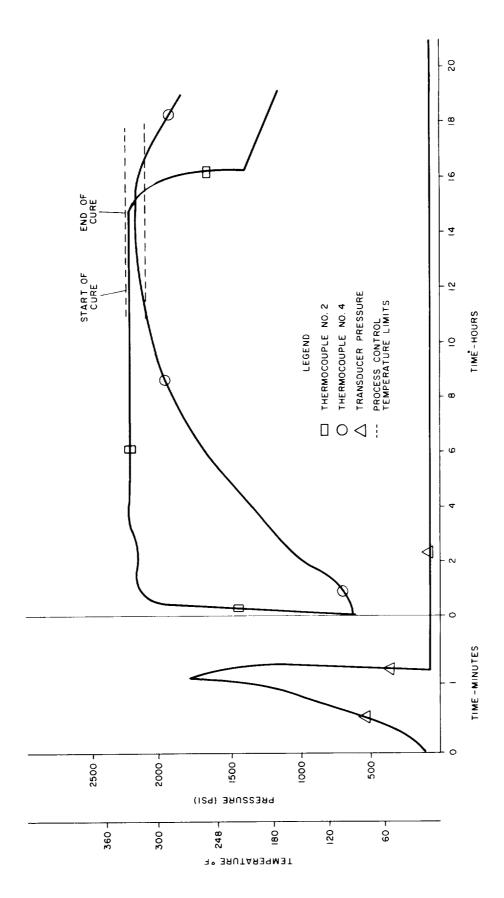
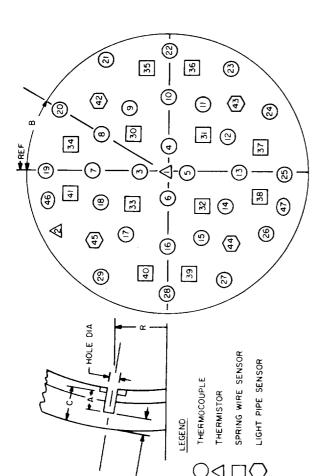


Figure 47. Bonding Graph, Nosecap No. 1

No.	No.	٧	8	U	×	×	DIA.
_	• 5	9950	0	2 : 45	Û	1,539	0.3.5
2		Э	330	2.918	3.0795	2.018	,
T/C							
3	NC5-6	1.710	С	7 O. V.	0.885	0.294	X 7 C
7	NC 5-5	1,703	66	1 1	0.885	6,301	248
Ş	NC8-6	1.508	180	2.003	688.0	665.0	248
9	NC 10-7	1.403	270	2,00%	0.885	0.691	248
7	NC5-7	1,710	0	2.010	1.9915	0.300	0.248
20	NC4 -6	1.810	30	2.010	1,9915	0.250	0.248
6	NC2 -4	1.909	09	2,008	1,9915	0.099	0.249
10	XC6 -4	1.608	06	2.009	1.9915	0.401	0.247
11	NC13-6	1,108	120	2.009	1.9915		
1.2	NC 14-2	1,009	150	2.610	1.9915	1,000	0.248
Ξ	XC 8 − 4	1,511	180	4 4	1.9915	6.497	0.247
14	NC12-1	1.212	210	2.010	1.9915		877 0
15	XC11-3	1.309	240	2.010	1.9915		3.00
16	NC 10-6	804.1	270	0.10.5			
1.7	NC15-4	0.907	300	2.010	1.4915		
18	NC15.5-1	0.345	330	5.009	1.9915	1.164	0.75 u
19	NC5-8	1.721	0	2.635	3.0795	300	276
2.0	NC2 - 7	1.912	08	1 .	1 '		
2.1	NC2 -6	1.916	09	١.	1 1	4 .	
2.2	NC6-5	1.616	90	2,013	3.0795		0.25
2.3	NC 13-4	1.111	120	2.011	3.0795	0.900	
24	NC 15-5	0,911	150	2,012	3,0795	1.10	0.249
2.5	NCS-7	516	180	21012	3.0795	965.0	0,247
26	XC4-5	1,813	210	2.012	3.0795	0, 199	0.248
7	NC11-4	1.318	240	5 U.S.	3.0795	0.695	0.247
5. E	NC (10-18)	1.413	270	2 3	3.0795	0.600	0.247
5.6	NC12-3	1,214	00	-1 -	3.0795	0.500	0.258
9 5	NC4-9	1.662	337.5	2.162	3.430	0.500	0.249
1 1	NC 7 - 3	1.46	107.5	2.103	3,430	0,702	0,249
3							
30	108	1.445	45	1.638	1,3275	0,193	0.021
<u>-</u>	57.7	24	135	1.638	1,3275	0.393	0.021
32	113	-1	225	. b36	1,3275	0.493	150.0
33	113	1.344	31.5	. 63.	1,3275	0.243	0,421
34	911	-1	1.5	- 5 36	655	6.193	0.021
35		5.3	. 5	3.6.16	2.655	1.093	0.001
96	120	0.43	105	966	6.655	(82.0	170
ć	6[]	1.542	165	. 635	2,055	0.090	[3]
38	113	1.491	195	46.4	559	0.140	0.021
33	116	143	255	98 9	2.655	0.493	0.07
O •7		1,243	285			0.393	0.021
7	112	1.343	345	. b 36	2.655	0.293	0.01
д. Н							
7.5		1.910	45	. N.2	2.655	0.102	0.248
<u>.</u>	- 1	1,661	135	Ī	7.655	0.352	570°0
7,7	125 41	1.558	225	balga	224 6		
					66.	O+.	7



The "X" dimensions logged do not inclus, ",au3" for the Teilon moisture barrier

Sensing Devices Installation and Measurement Log, Nosecap No. 1 Figure 48.

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SPRING-WIRE SENSOR INSTALLATION

Installed Date: 8/2/65

NOSECAP NO. 1

												 -
Hole Number	30	34	33	41	31	40	39	32	38	37	36	35
Distance Surface to End of Tube	0.200	0.199	0.299	0.299	0.402	0.398	0.500	0.498	0.146	0.099	0.897	1.101
Shim Thick- ness	0.063	0.063	0.058	0.061	0.063	0.061	0.062	0.068	0.055	0.057	0.058	0.063
Remain- ing Thick- ness "X"	0.190	0.190	0.290	0.290	0.390	0.390	0.490	0.490	0.140	0.090	0.890	1.090
Hole Depth	1.445	1.443	1.344	1.343	1.245	1.243	1.143	1.143	1.491	1.542	0.743	0.543
Total Thick- ness of Nosecap	1.635	1.633	1.634	1.633	1.635	1.633	1.633	1.633	1.631	1.632	1.633	1,633
Hole Number	30	34	33	41	31	40	39	32	38	37	36	35
r Length To End of Knot	1.503	1.503	1.398	1.401	1.305	1.300	1.203	1.208	1.545	0.599	0.798	0.603
Sensor To End of Tube	1,498	1.497	1.393	1.395	1.296	1.296	1.195	1.203	1.540	0.590	0.794	0.595
Sensor Number	109	110	111	112	113	114	116	117	118	119	120	121

FORM RE2-2

Figure 49. Spring-Wire Sensor Installation

LIGHT PIPE LOCATION

ASSEMBLY NO. NC No. 1

	_ 	,	 .		
STANCE	Post Instal-	29 К	31.5 K	33.25K	31.5 K
SENSOR RESISTANCE	Pre-Instal- lation	29 K	33 K	35 K	33.5 K
WASHER	Shim Thickness	0.243	0.244	0.249	0.241
10C)	X	0.102	0.352	0.451	0.250
ASSEMBLY (MAT'L NO. 10C)	Depth Meas.	0.248 1.910 0.102	1.661	1.558	0.250 1.762 0.250
LY (MAT	Hole Diam. Depth Jumber Meas. Meas.	0.248	0.248	0.249	0.250
ASSEMB	Hole Diam. Number Meas.	42	43	44	45
		0.248	0.248	0.249	0.250
14C)	"M" Length Measured	1.964	1.716	1.618	1.814
LIGHT PIPE (MAT'L NO. 14C)	Serial Mat'l "L" Length "M" Length Diam. Number No. Measured Measured Meas.	2.154	1.906	1.808	2.004
r PIPE	Mat'l 'No.	14	14	14	14
LIGH	Serial Mat'l Number No.	1.P 99	86	06	91

FORM RE3-2

Figure 50. Light Pipe Location

FORM RE1

THERMOCOUPLE LOCATION

1965

DATE Aug. 17,

ASSEMBLY NO. NC NO.

RESISTANCE	Alumel Leakage	8													
	Chromel Leakage	8													
FINAL ELECTRICAL	Reverse	19.86	18.37	19.35	19.80	21.15	20.06	18.87	18.45	RE	19.80	21.01	20.91	21.26	20.94
FINAL	Forward	19.86	18.37	19.35	19.80	21.15	20.06	18.87	18.45	SPARE	19.80	21.01	20.91	21.26	20.94
WASHER	Shim Thick- ness	0.230	0.239	0.232	0.239	0.231	0.230	0.235	0.233	0.237	0.236	0.239	0.245	0.237	0.234
.10C)	"X"	0.294	0.301	0.495	0.601	0.300	0.200	0.099	0.401	0.901	1.001	0.497	0.798	0.701	0.602
(MAT'L No.10C)	Depth Meas.	1.710	1.703	1.508	1,403	1.710	1.810	1.909	1.608	1.108	1.009	1.511	1.212	1.309	1.408
SEMBLY (MA	Diam. Meas.	0.248	0.248	0.248	0.248	0.248	0.248	0.249	0.247	0.248	0.248	0.247	0.248	0.248	0.248
ASSEM	Hole Number	3	4	5	9 -	2	5 I	6	- 10	5 11	12	13	- 14	15	16
	Diam. Meas.	0.246 0.248	0.249	0.248	$\begin{vmatrix} 0.247 - 0.248 \\ 0.248 \end{vmatrix}$	0.247 - 0.249	249 249	0.247 0.249	0.246 - 0.247	0.248- 0.2485	0.247 - 0.2485	0.246-0.248	0.248-	0.246 - 0.248	0.247 0.249
(MAT'L No.)	"M" Length Measured	1.752	1.754	1.552	1.454	1.753	1.852	1.953	1.653	1.157	1.057	1.562	1.269	1.358	1.454
THERMOCOUPLE (MA	"L" Length Measured	1.942	1.944	1.742	1.644	1.943	2.042	2.146	1.843	1.347	1.247	1.752	1.459	1.548	1.644
THERM	Serial Number	NC 5-6	NC 5-5	NC 8-6	NC10-7	NC 5-7	NC 4-6	NC 2-4	NC 6-4	NC13-6	NC14-2	NC 8-4	NC12-1	NC11-3	NC10-6
		3C	30	30	4C	30	15C	30	3C	30	30	30	30	30	30

Figure 51

THERMOCOUPLE LOCATION

No. NC ASSEMBLY NO.

2 (Sheet No.

Chromel Alumel Leakage Leakage RESISTANCE 8 3 ELECTRICAL Forward Reverse 21.38 18.85 19.37 98 20.9520.79 21,19 21.2518.83 21.9016.13 15,09 18 SPARE SPARE FINAL 20.79 16.13 15.09 21.38 20.95 21,19 21,25 18.85 21.90 18.83 18.98 37 19. Shim Thick-WASHER 0.250 0.2520.230 0.220 0.224 0.230 0.229 0.236 0.224 0.229 0.226 0.226 0.227 ness N/A0.101 0.096 0.496 (MAT'L No.10C) 1.103 1.164 0.900 0.1990.695 0.294 0.397 1,101 0.600 0.800 0.500 "X" Depth Meas. 0.911 1.916 1.616 1.516 0.845 1.721 1,111 1.813 318 0.249 1.662 0.907 1,912 1,413 1.214 H Diam. Meas. 0.2490.2490.248 0.248 0.247 0.247 0.2480.249 0.247 0.248 0.2480.247 0.247 ASSEMBLY Hole Number 2018 23 25 26 19 28 29 17 2224 21 27 46 0.2475 - 0.24850.2465 - 0.2490.2485 - 0.24950.2475 - 0.24850.245 - 0.2470.246 - 0.2480.247 - 0.248 $0.247 - 0.248 \mid$ 0.245-0.246 - 0.2480.246 - 0.247Meas. 0.249 - 0.2480.245 - 0.249Diam. 0.247"M" Length Measured (MAT'L No.) 0.971 0.907 1.658 1.152 1.5521.356 1.757 1.955 1.948 0.959 1,854 1,255 1.8531.451 "L" Length Measured THERMOCOUPLE 1,161 1.097 1.342 2.0441.546 2.1451.947 2.138 1.848 1.149 1.445 1.742 1.641 2.043 Serial Number 5-8 2-6 6-5 NC15-4 2-7 4-9 NC13-4 NC15-5 8-7 4-5 NC11-4 NC10-8 3C NC12-3 NC15. 5-1 NC NC NC NC NC NCNC

3C

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0.247

1.607

1.797

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NC

4C 3C

3C

3C

3C

15C

APPENDIX A

PHENOLIC NYLON NOSECAP

DRAWING LIST

Drawing Number	Revision	Title
LX-410115	G	Assembly - Phenolic Nylon Nosecap
LE-410116	Α	Substructure
LD-410117	D	Thermocouple Detail Assembly
LD-410118	E	Optical Light Pipe Abl. Sensor Assy.
LD-410119	D	Spring Wire Abl. Sensor Assy.
LC-410120	Α	Ablator
LC-410121		Cable Clamp
LB-410122		Drill Jig, Spring Wire Abl. Sensor
LB-410123		Spacer, Spring Wire Abl. Sensor
LB-410124		Retaining Washer
LB-410125		Bond Tensile Test Specimen
LB-410126		Bond Shear Test Specimen
LD-410127	Α	Nosecap Supporting Form
LD-410128	D	Arc-Jet Specimen
LC-410129		Plug Bonding Specimen
LD-410271		Plug Density Variation, Arc-Jet
		Specimen
LD-410272		Constant Plug Density, Arc-Jet
		Specimen
LB-410274		Thermal Shock Specimen
LB-410275	A	Ablation Sensor, Arc-Jet Specimen
LA-410276	A	Mount, Arc-Jet Specimen
LC-410277		Thermocouple, Arc-Jet Specimen
LC-410278		Systems Test, Arc-Jet Specimen
LC-410279		Spring Wire Abl. Sensor, Arc-Jet
		Specimen
LB-410309	Α	Calorimeter, Arc-Jet Specimen
LB-410310	Α	Calorimeter Holder
LB-410314		Calorimeter, Materials Performance Arc
		Specimen
LB-410317	С	Materials Performance Arc Specimen
LD-410326		Uninstrumented Arc-Jet Specimen
LC-410327	Α	Optical Light Pipe Abl. Sensor, Arc-
		Jet Specimen
LC-410328		Certified Material L/P Test, Arc-Jet
		Specimen
LC-410331		Plug Recession, Arc-Jet Specimen
LC-410332		Plug Installation, Arc-Jet Specimen
LA-410333		0.020 Diam. Tube Locating Fixture
LC-410334		Thermocouple and Plug Recession Test, Arc-Jet Specimen
LA-410339		Terminal Strip
LB-410372		Hemispherical Arc-Jet Specimen
LC-603899		Temperature Sensor, Wiring Schematic
LC-604108		Ablation Sensor, Nosecap Wiring
		Diagram

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APPENDIX B

SUMMARY OF MEASUREMENTS FOR REENTRY E FLIGHT NOSECAP (NO. 2

CHANNEL NO. 13, 14.5 KC

NOSECAP ABLATION SENSORS

	Remarks																						
ATION	٥	In.	ı	ı	ı	I	ı	2.655	=	=	=	1.3275	=	:	=	2.655	:	:	÷	£	:		:
SENSOR LOCATION	Φ.	Deg.	ı	ı	ı	I	ı	45	135	225	315	45	135	225	315	15	75	105	165	195	255	285	345
SE	X	In.	1	ı	ı	1	ı	. 100	.349	. 452	. 247	. 203	.402	. 505	. 291	. 199	. 095	. 895	. 747	. 148	. 504	.398	.297
	Sensor	No.	1	1	ı	i	ı	42	43	44	45	30	31	32	33	34	35	36	37	38	39	40	41
	Sensor	Type	Ή.	Cal. Full	Ξ.	Cal. Full	Cal. Half	Light Pipe) =	:	:	Spring Wire	=		=======================================	=======================================	1.	:	:	:	=	:	=
	Switch	Position	Ħ	2-3	4	5	9	-17-	8-18-28	-19-	-20-	11	12	13	14	15	16	21	22	23	24	25	26

(1) "X" dimension is sensor measurement point and includes .010 in. in addition to NOTE:

material thickness for spring wire sensors. ϕ is angular position relative to tower side of yaw axis looking forward. ρ is radial location relative to thrust axis. (3)

CHANNEL NO. 14, 22 KC

NOSECAP CHROMEL-ALUMEL THERMOCOUPLE

į		Remarks																					
	ATION	9	.11.	ı	ı	ı	ı	ŀ	.885		1.9915	=	:	:	3.0795		1.9915	3.0795	=	3.43		ı	
	SENSOR LOCATION	φ	DCB.	1	ı	ı	1	ı	90	270	180	240	300	330	0	210	150	09	06	187.5		1	
	SE	"X" In		1	1	1	ı	ı	.401	.602	. 501	. 702	1.102	1.206	.301	. 199	1.003	. 100	.399	. 700	ı	ı	
		Sensor		1	ı	ı	1	ı	4	9	13	15	17	18	19	26	12	21	22	47	Cal. Ref.	1	
		Sensor	13 FC	Cal. Zero		Cal. Half	Cal. Full		Thermocouple	=	:	=	Ξ	Ξ	Ξ	=	Ξ		=	Ξ	=	**	
		Switch Position		H	2-3	4	ນ	9	7-22	- 1	9-24	10-25		12-27	13-28	- 1	1	16	17	18	19	20	

CHANNEL NO. 16, 40 KC

MISCELLANEOUS

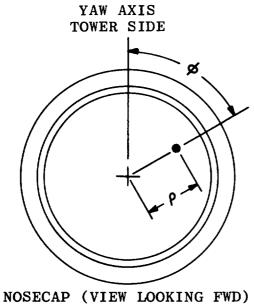
							ring)	r ring)	ring)	ring)																			
	Kemarks						IJ	in.	78 in. (fwd.	10 in. (fwd.							T/M Deck	Ξ	Ξ	=	:	=	:	:	Ξ				
	In.	1	ı	1	ı	t	ı	1	1	ı	0	3.0795	1	ı	i	ı										ı	ı	1	1
Sensor Location	Deg.	1	1	ı	ı	1	180	180	180	180	0	330	ı	1	ı	ı										1	1	1	ı
Se ₁	In.	ı	ı	•	1	1	ı	ı	ı	ı	1.524	1.985	ı	ı	1	1		7	က	4	ಬ	9	7	œ	6	ł	ı	ı	ı
Sensor	Number	ı	1	ı	ı	ı	101	102	103	104	ᆏ	2	ł	i	1	ı	Thermistor	:	:	:	:	:	:	:	÷	ı	ı	ı	ı
	Measurement	Cal. Zero	Full Scale	4		Cal. Half	A/B Thermocouple	A/B Thermocouple	A/B Thermocouple			N/C Thermistor 2	~	VSWR Direct Rev		VSWR Delayed Rev	Xmtr. Delay Temp.	Cold Junction 1	Xmtr. Direct Temp.		T/R Temperature	Cold Junction 3	Direct VSWR Temp.	Delay VSWR Temp.	_	+300 V Monitor	Unstable 28 V	Stable 28 V	Zero
Switch	Position	1	2-3	4	5	9	7	œ	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29-30

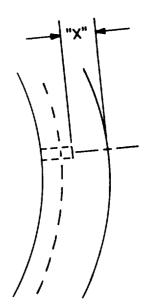
*Relative to aft end of afterbody

CHANNEL NO. 18, 70 KC

NOSECAP CHROMEL-ALUMEL THERMOCOUPLES

Suttch Sensor "X" \$\overline{\phacesty}\$ \$\ov							
sition Type No. In. Deg. In. Cal. Zero				Sen	sor Locat	ion	
Cal. Zero -3 Cal. Full -2 Cal. Half -22 Thermocouple -24	Switch	Sensor	Sensor		0		Remarks
Cal. Zero	Position	Type	No.	In.	Deg.	In.	
-3 Cal. Full	+	: ا	ı	1	ı	ı	
Cal. Half	2-3	٦.	ı	ı	1	ı	
Cal. Full	4		ı	ı	ı	ı	
Cal. Half -22 Thermocouple 3 .302 0 -23 Thermocouple 5 .501 180 -24 " 7 .299 0 125 " 8 .200 30 -26 " 9 .099 60 -27 " 10 .400 90 -27 " 14 .801 210 -29 " 23 .501 337.5 330 " 24 1.205 150 -30 " 27 .701 240 -30 " 27 .701 240 -30 " 27 .701 240 -30 " 27 .701 240 -30 " 28 .601 270 -30 " 28 .601 270 -30 " 29 .301 300 -30 " 30 .301	5		ı	ı	ı	ı	
-22 Thermocouple 3 .302 023	9		ı	ı	ı	1	
-23 "" 7 . 299 0 124 " 8 . 200 30 125 " 9 . 099 60 60 -27 " 10 . 400 90 -28 " 14 . 801 210 -29 " 23 . 902 120 330 " 46 . 501 337.5 330 " 27 . 701 240 -10 . 20 . 601 270 -10 . 20 . 601 270 -10 . 20 . 601 270 -10 . 20 . 601 300 -10 . 20 . 601 300	7-22	Thermocouple	က	.302	0	. 885	
-24 " 299 0 125 " 200 30 30 -26	8-23	:	2	. 501	180		
-25 8200 30	- 1	:	7	. 299	0	•	
-26 " 9 .099 60 .277 " 10 .400 90 .278	- 1	•	80	. 200	30	E	
-27 " 10 .400 90 -28	- 1	ε	6	660.	09	=	
-28 " 801 210 270 270 23 .902 120 3. -29 " 602 270 270 23 .902 120 3. -30 " 24 1.205 150 3. 25 .502 180 270 -27 .701 240	- 1	፡	10	. 400	06		
-29 " 602 270 23 -23 .902 120 3		:	14	.801	210		
-30 ". 46 . 501 337.5 3. 46 . 501 337.5 3. 24 1.205 150 3. 25 . 502 180 27 . 701 240 28 . 601 270 SPARES Thermocouple 11 .902 120 1. 20 .097 30 3.	- 1	:	16	.602	270	-	
#6 .501 337.5 3. 24 1.205 150 3. 25 .502 180 27 .701 240 28 .601 270 SPARES Thermocouple 11 .902 120 1. 20 .097 30 3.	- 1	Ξ	23	. 902	120	3.0795	
Thermocouple 11 .905 150 3. 24 1.205 150 3. 25 .502 180 27 .701 240 28 .601 270 SPARES Thermocouple 11 .902 120 1. 20 .097 30 3.		Ξ.	46	. 501	•	3.43	
Thermocouple 11 .902 180 Thermocouple 11 .902 120 1. Thermocouple 11 .902 120 1. 25 .502 180 26 .601 270 SPARES 27 .701 240 270 .701 240 SPARES SPARES 29 .902 120 1. 30 3.	17	:	24	1.205	150	3.0795	
Thermocouple 11 .902 120 1. Thermocouple 11 .902 120 1. Thermocouple 20 .097 30 3.	18		25	. 502	180	:	
Thermocouple 11 .902 120 1. Thermocouple 11 .902 120 1. Thermocouple 20 .097 30 3.	19	-	27	.701	240	=	
Thermocouple 11 .902 120 1 20 300 3.	20	፡	28	.601	270	:	
SPARES 11 .902 120 1. 20 .097 30 3. 29 .801 300	21	:	1				
11 .902 120 1. 20 .097 30 3. 29 .801 300				SPARES			
20 .097 30 3. 29 .801 300	:	Thermocouple	11	. 902	120	1.9915	
	!	: :	7 70 7 80 7 80	. 801	300	3.0785	





DEFINITIONS:

- IS ANGLE RELATIVE TO TOWER SIDE OF YAW AXIS
- IS RADIAL DISTANCE FROM THRUST AXIS TO THE SENSOR INSTALLATION HOLE
- " X" IS SENSOR MEASUREMENT POINT RELATIVE TO AND PERPENDICULAR TO THE NOSECAP FRONT SURFACE

SUMMARY OF MEASUREMENTS FOR BACKUP NOSECAP NO. 1

CHANNEL NO. 13, 14.5 KC

NOSECAP ABLATION SENSORS

	Remarks																					
tion	$_{\mathrm{In.}}^{ ho}$	1	,	ı	1	ı	2.655	=	£	=	1,3275		Ξ	Ξ	2.655		:		:	=	=	=
Sensor Location	φ Deg.	B	ı	ı	i	i	45	135	225	315	45	135	225	315	15	75	105	165	195	255	285	345
Se	''X'' In.]	ı	ı	1	1	. 102	.352	. 451	.250	. 200	.402	. 498	. 299	. 199	1.101	. 897	660.	. 146	. 500	. 398	. 299
	Sensor No.		ı	1	1	1	42	43	44	45	30	31	32	33	34	35	36	37	38	39	40	41
1 1 2 2	Sensor	Cal. Zero	Cal. Full	Ξ.	Cal. Full	Cal. Half	Light Pipe	**		:	Spring Wire		:	1	11	11	44		**	••		
A	Position	1	2-3	4	വ	9	7-17-27	- 1	9-19-29		11	12	13	14	15	16	21	22	23	24	25	26

"X" dimension is sensor measurement point and includes .010 in. in addition (1) NOTE:

to material thickness for spring wire sensors. ϕ is angular position relative to tower side of yaw axis looking forward. ρ is radial location relative to thrust axis. (3)

CHANNEL NO. 14, 22 KC

NOSECAP CHROMEL-ALUMEL THERMOCOUPLE

	Remarks																				
ion	ρ In.	-	1	•	1	i	. 885	:	1.9915	:	=	=	3.0795	:	1.9915	3.0795	:	3.43	1	1	1
Sensor Location	$\overset{oldsymbol{\phi}}{\operatorname{Deg.}}$	ı	ı	ı	ı	ı	90	270	180	240	300	330	0	210	150	09	06	187.5	ı	ı	ı
	"X" In.		ı	ı	ı	ı	.301	.601	. 497	. 701	1.103	1.164	. 294	. 199	1.001	960.	.397	. 702	ı	1	t
:	Sensor No.		ı	1	f	i	4	9	13	15	17	18	19	26	12	21	22	47	Cal. Ref.	1	1 1
	Sensor Type	1	Cal. Full				Thermocouple	:	**	**	*		*	-	II-	*	** *-	=	**		=
	Switch Position	1	2-3	4	5	9	- 1	- 1	9-24	10-25	11-26	12-27	ı	14-29	15-30	16	17	18	19	20	21

CHANNEL NO. 16, 40 KC

MISCELLANEOUS*

	Remarks	*Same as for flight	ו מ ב	6.1	Thermistons 1 and 9	ד מוומ											T/W Deck	1000 ==	*	=	=	Ξ	Ξ	Ξ	=				
i o	In.	ı	ı	I	ı	ı	ı	ı	ı	ı	0	3.0795) ; ; I	1	ı	1										ı	ı	ı	ı
Sensor Location	φ Deg.	1	1	ı	1	ı	180	180	180	180	0	330	I	ı	i	ı										ı	1	ı	ı
Sen	"X". In.	ŀ	1	1	ı	ı	I	1	ı	ŀ	1.539	2.018	1	ı	ı	I	or 1		က	4	വ	9	7	∞	6	ı	i	ı	1
	Sensor Number	ı	ı	ı	ı	ı	101	102	103	104	H	2	ı	ı	ı	ı	Thermistor	:	:	=	:	:	:	:	:	ı	1	t	
	Measurement			Half Scale	•	Cal, Half	A/B Thermocouple	A/B Thermocouple	A/B Thermocouple		_	N/C Thermistor 2	VSWR Direct Fwd	VSWR Direct Rev		VSWR Delayed Rev	Xmtr. Delay Temp.	\sim	Xmtr. Direct Temp.	FAT	T/R Temperature	$\overline{}$	Direct VSWR Temp.	VSWR 7	Cold Junction 2	+300 V Monitor	Unstable 28 V	œ	Zero
	Switch Position	H	2-3	4	5	9	7	∞	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	29-30

CHANNEL NO. 18, 70 KC

THERMOCOUPLES	
CHROMEL-ALUMEL	
NOSECAP	

	Remarks																						
ion	ρ In.	!	1	1	ı	ı	.885		1.9915	=	:	=	=	:	3.0795	3.43	3.0795	:		£	I		1.9915 3.0795
Sensor Location	φ Deg.	ı	ı	i	ı	ì	0	180	0	30	09	90	210	270	120	337.5	150	180	240	270	ı		120 30 300
Sens	"X" In.	ı	1	1	1	1	. 294	. 495	.300	. 200	660.	.401	. 798	.602	006.	. 500	1,101	. 496	.695	009.	ı	SPARES	.901 .101 .800
	Sensor No.	•	ı	ı	1	ı	က	5	7	8	6	10	14	16	23	46	24	25	27	28	<u> </u>		11 20 29
	Sensor Type	Cal. Zero	-	1.	Cal. Full	1.	Thermocouple	*	*	•	=	:	**	**	:	:	:	:	•	:	:		Thermocouple "
	Switch Position	1	2-3	4	5	9		- 1		- 1	11-26					16	17	18	19	20	21		111

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		<u> </u>
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